

Lecture

is available on

<http://www.astro.uni-bonn.de/~bertoldi/wiki/Radiolnterferometry>

Interferometric Calibration & Imaging

Peter Schilke, MPIfR

Editing and calibration

- An Interferometer measures the visibility of antenna pairs (or on baselines)

$$V_{ij}(t) = \iint A_v(l, m) I_v(l, m) e^{-2\pi i(u_{ij}(t)l + v_{ij}(t)m)} dl dm$$

- the term $(ul+vm)$ gives the geometrical phase difference between the phase center (where the fringes are stopped) and the source
- the phase determines the location of a source
- the amplitude the strength

Editing and calibration

- Editing is basically just throwing out of bad data
- ...so one either has to have good automatic quality checks (phase jumps) and/or good visualization tools
- Calibration is correcting the data for measurement errors

Measured in practice

$$\tilde{V}_{ij}(t) = G_{ij}(t) V_{ij}(t) + \epsilon_{ij}(t) + \eta_{ij}(t)$$

where

$G_{ij}(t)$ is a baseline dependent complex gain

$\epsilon_{ij}(t)$ is a baseline dependent complex offset

$\eta_{ij}(t)$ is a stochastic noise term

Calibration

- One calibrates by observing a source of known structure – ideally, a point source – once in a while
- “once in a while” depends on the stability of the system
 - instrumental part
 - atmospheric part
- Compromise between calibrating often (good data quality) and calibrating rarely (observing efficiency)

Atmospheric stability

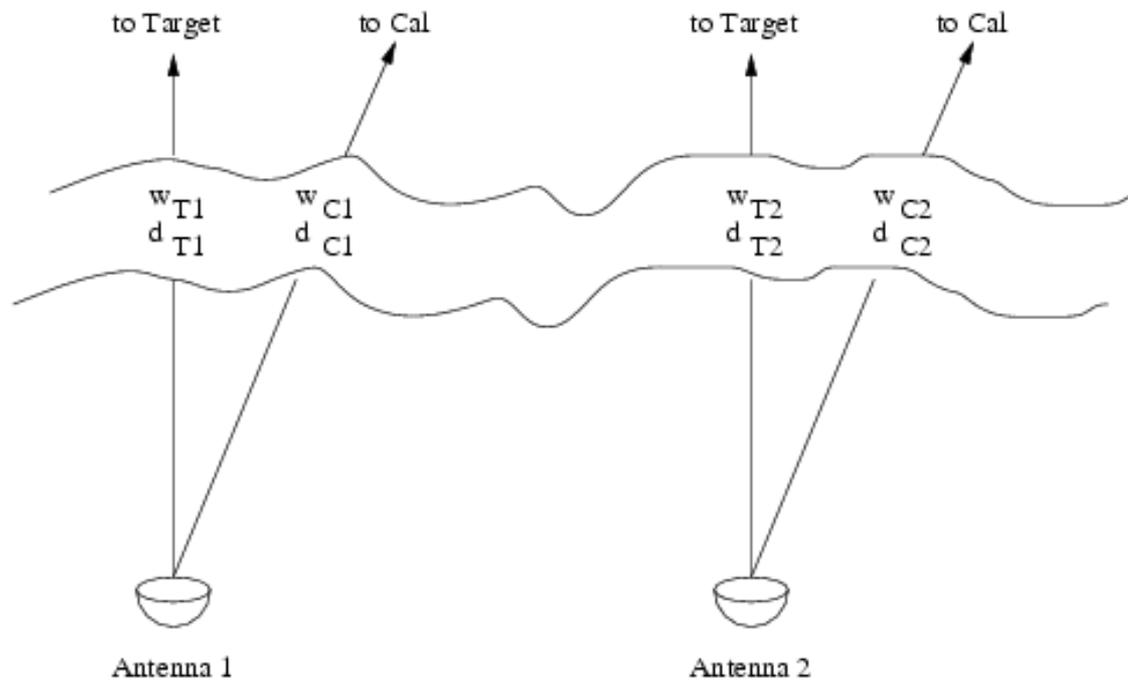
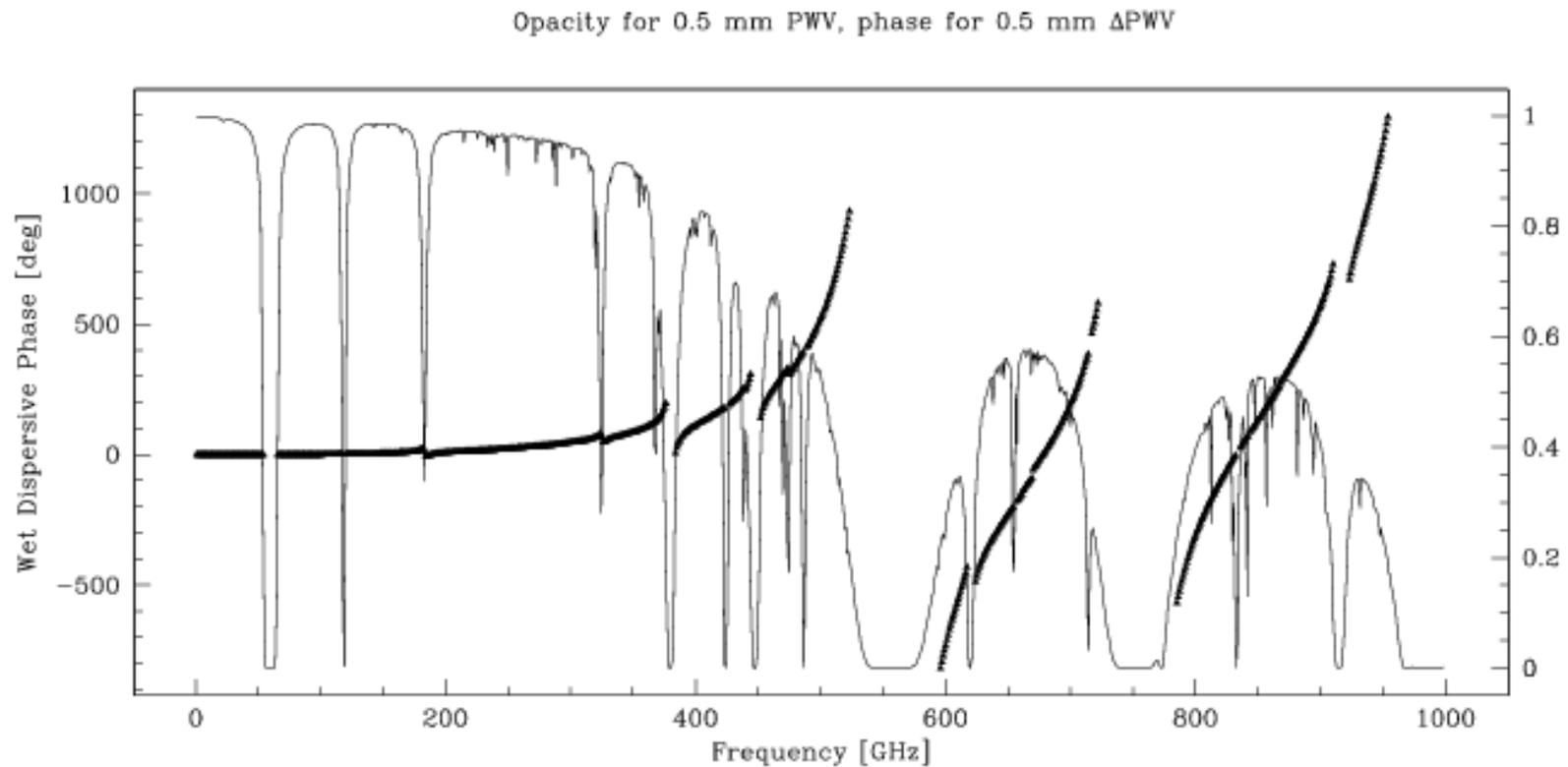


Figure 3: Schematic showing the water vapor columns (eg, w_{C1}) and dry delays (eg, d_{C1}) toward the calibrator and the target sources above antennas 1 and 2.

Calibration

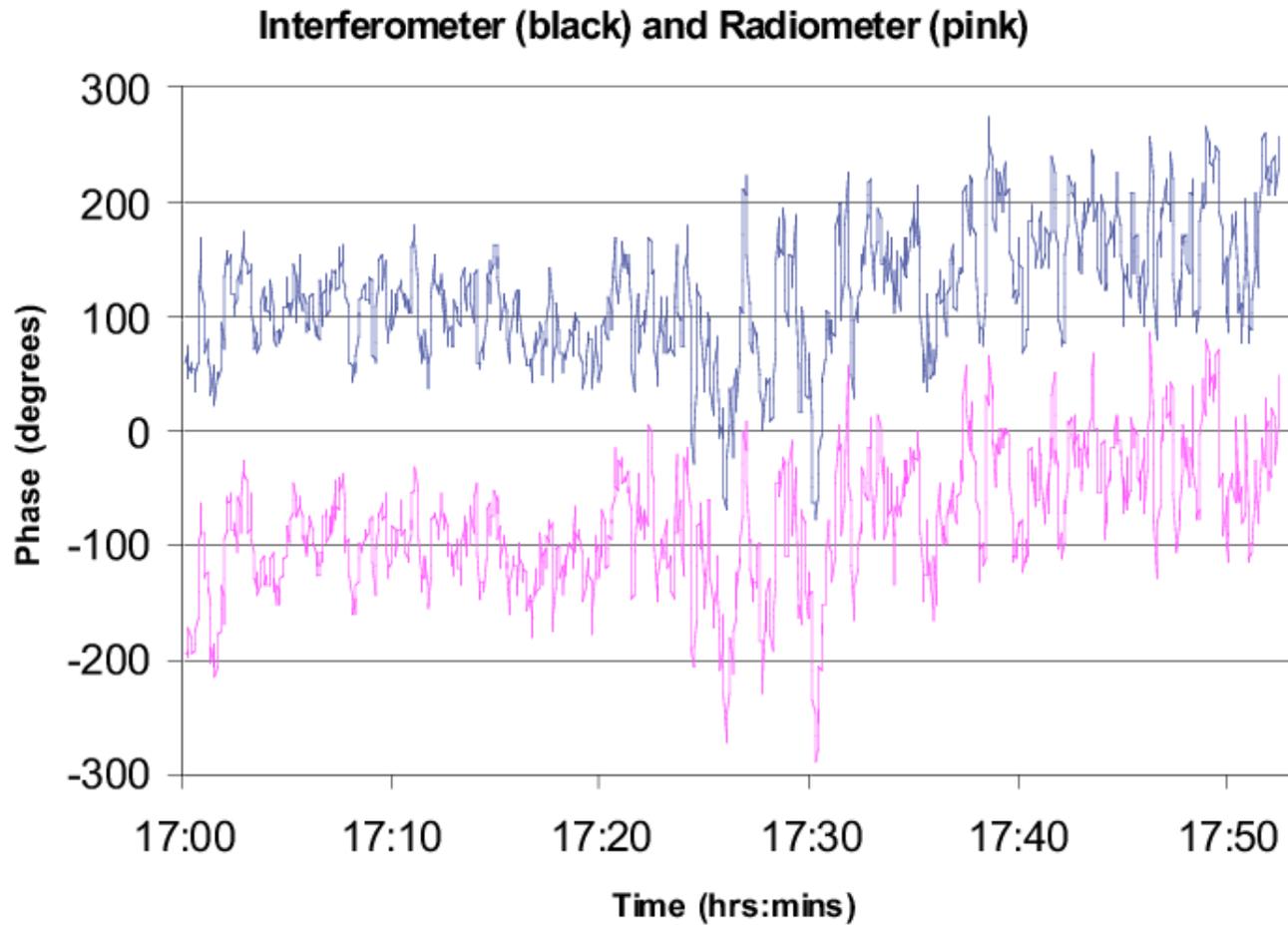
- Other compromises:
 - calibrator source should be strong
 - to get good S/N
 - nearby
 - to minimize dead time for moving telescope
 - to have same atmospheric conditions

Phase dispersion



nondispersive part: $\Delta \phi \propto \nu$

Alternative: radiometric correction



Amplitude and phase calibration

- **Baseline based**
 - natural – visibilities are measured on baselines
 - tedious – for N antennas there are $N(N-1)/2$ baselines, e.g. for ALMA with $N=50$ there are 1225 baselines
 - not possible to do visually
- **Antenna based**
 - most errors ARE antenna based
 - choice for more than 5-6 antennas out of necessity

Calibration – baseline based

- For a point source with complex visibility S (i.e. Amplitude is S Jy and phase is 0), one gets

$$G_{ij}(t) = \frac{\tilde{V}_{ij}(t)}{S}$$

if

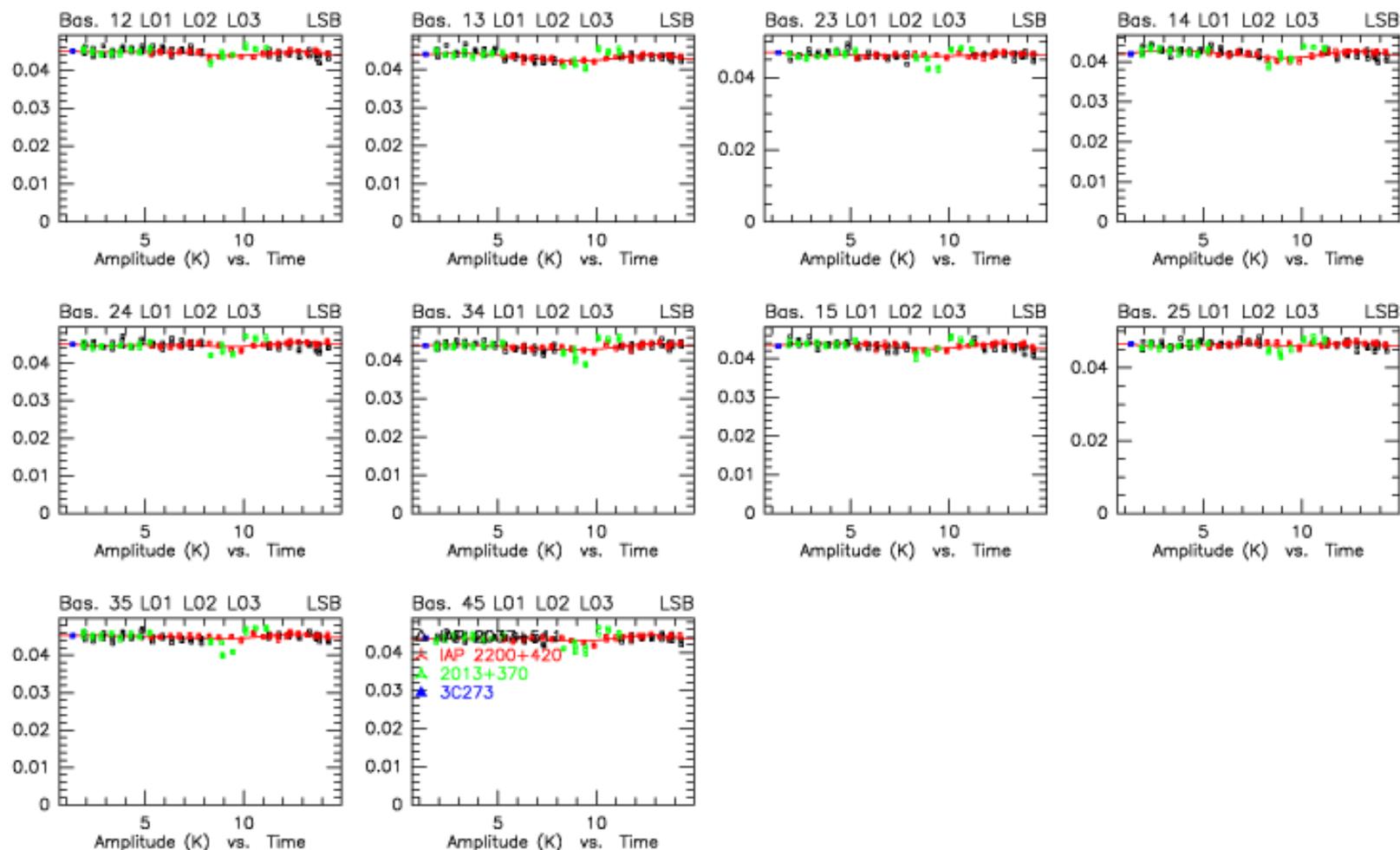
$\epsilon_{ij}(t)$ and $\eta_{ij}(t)$ *can be neglected*

Phase and Amplitude calibration

- This $G_{ij}(t)$ is measured from time to time – for each baseline – interpolated in time and applied to the source
- sometimes one uses more than one calibrator (left and right of the source)
- For high frequencies, there often are no strong calibrators closeby – phase transfer can then be employed

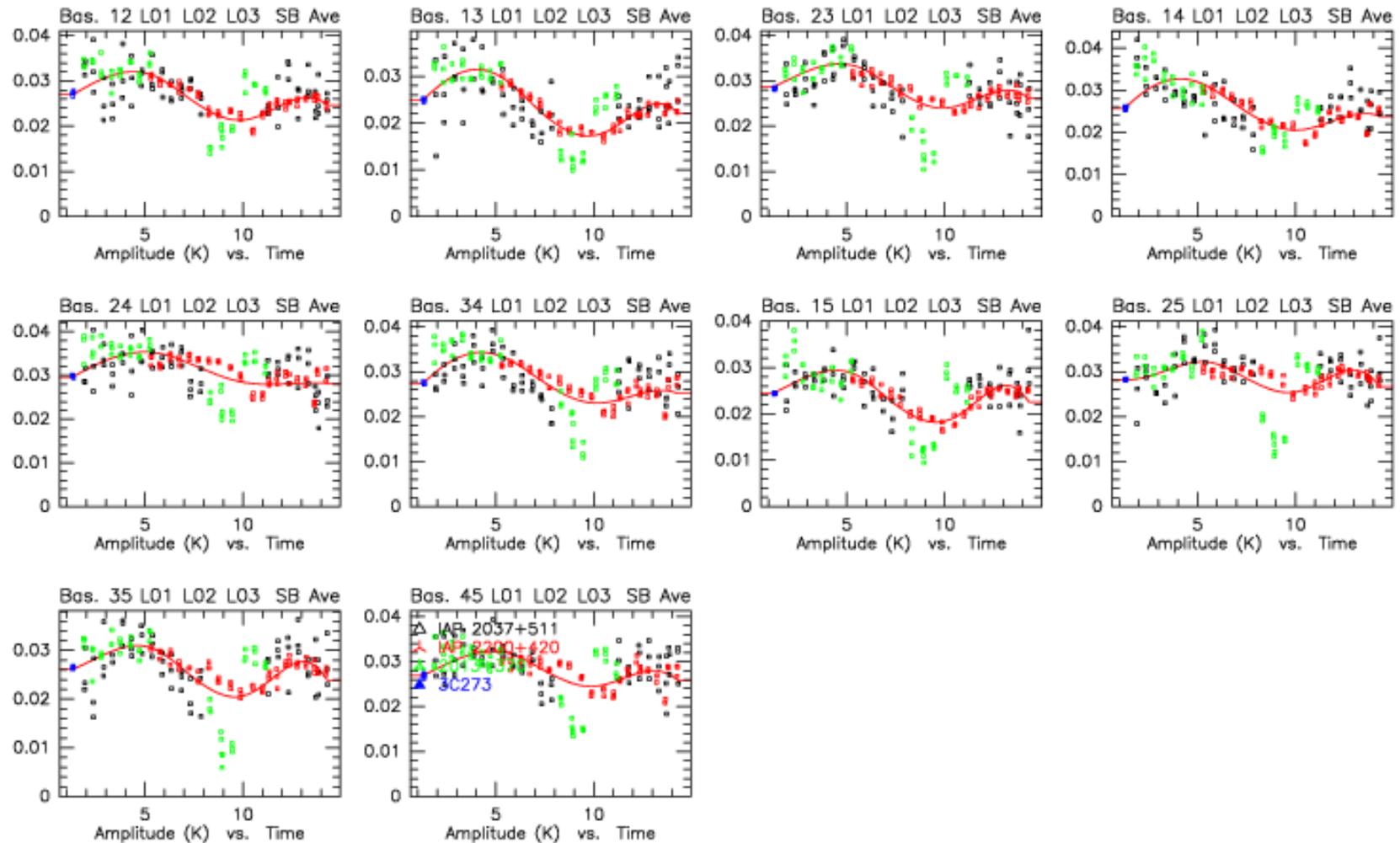
Example: PdB amplitude calibration - 3mm

W: 11-VV UTC = 19-MAR-1998 09:11:50 = schirke@claraip N15N03W09W12E10 Scan Avg.
Am: Scaled 188 9866 H100 3C273 P CORR N2H+(10) 5C2 14-MAR-1998 01:16 .6 Vect.Avg.
Ph: Rel.(A) Atm. 1173 718 H100 IAP 2037+511 P CORR N2H+(10) 5C2 14-MAR-1998 14:19 5.5



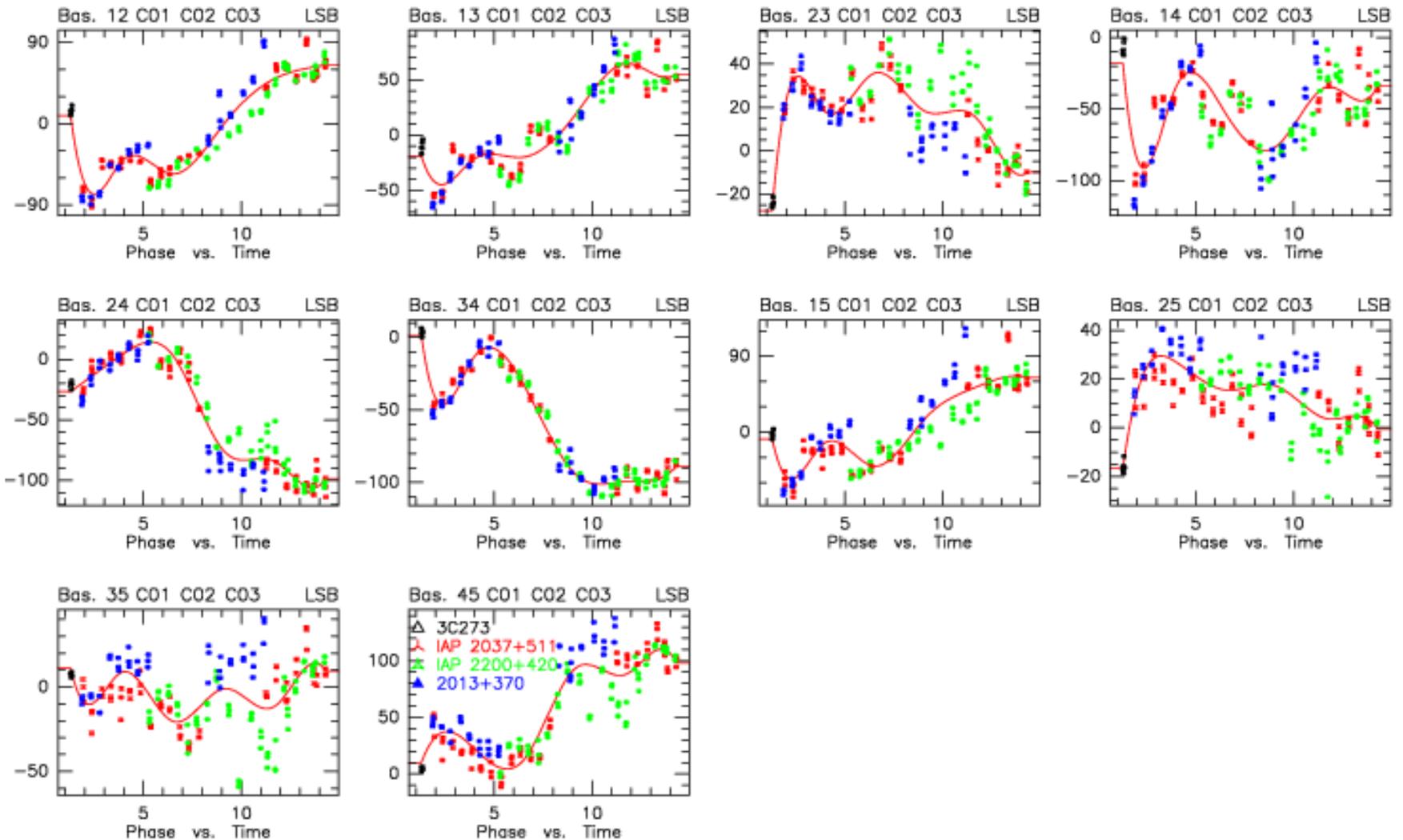
PdB amplitude calibration - 1mm

W. 11-VV CLIC - 19-MAR-1998 09:12:20 - schinke@clomp N13N03709W12210 Scan Avg.
 Am: Scaled 1372 9866 H100 3C273 P CORR CO+(21) 5C2 14-MAR-1998 01:16 .6 Vect.Avg.
 Ph: Rel.(A) Atm. Ext. 2357 718 H100 IAP 2037+511 P CORR CO+(21) 5C2 14-MAR-1998 14:19 5.5



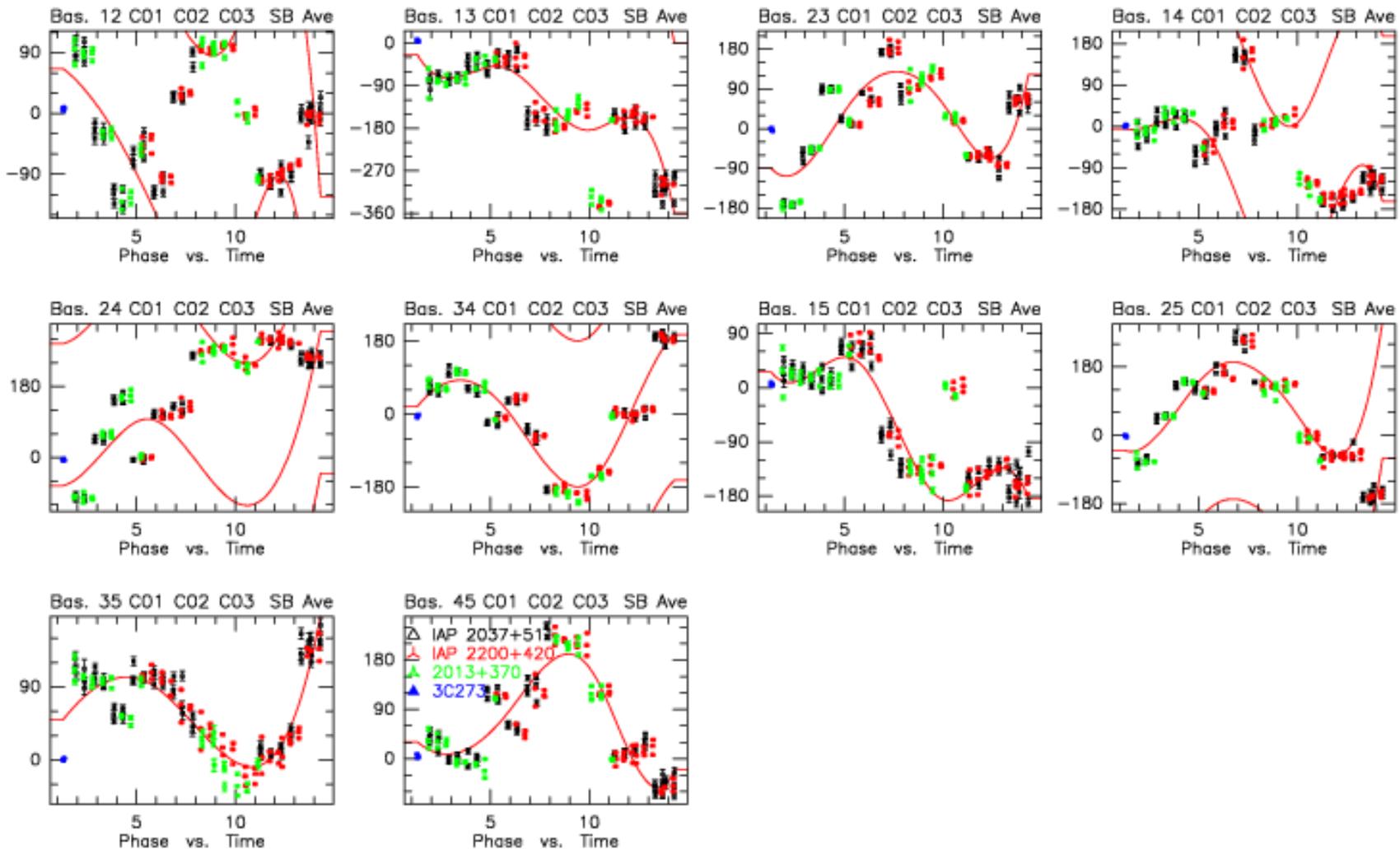
PdB phase calibration - 3mm

Arr: Abs. 188 9866 H100 3C273 P CORR N2H+(10) 5C2 14-MAR-1998 01:16 .6 Vect.Avg.
 Ph: Abs. Atm. 1173 718 H100 IAP 2037+511 P CORR N2H+(10) 5C2 14-MAR-1998 14:19 5.5



PdB phase calibration - 1mm

Am: Abs. 1372 9866 H100 3C273 P CORR CO+(21) 5C2 14-MAR-1998 01:16 .6 Vect.Avg.
 Ph: Abs. Atm. Ext. 2357 718 H100 IAP 2037+511 P CORR CO+(21) 5C2 14-MAR-1998 14:19 5.5



Antenna based calibration

$$G_{ij}(t) = g_i(t) g_j^*(t) g_{ij}(t)$$

- g_i and g_j are the antenna based gains, g_{ij} is the baseline dependent residual (closure error), which usually is in the 1% range
- this leads to the amplitude and phase equations

$$A_{ij}(t) = a_i(t) a_j^*(t) a_{ij}(t)$$
$$\Phi_{ij}(t) = \phi_i(t) - \phi_j(t) + \phi_{ij}(t)$$

Antenna based calibrations

- real and measured visibilities are then

$$V_{ij}(t) = A_{ij} e^{i\phi_{ij}}$$

$$\tilde{V}_{ij}(t) = \tilde{A}_{ij} e^{i\tilde{\phi}_{ij}}$$

for a point like calibrator with flux density S

$$A_{ij} = S \text{ and } \phi_{ij} = 0$$

and

$$\tilde{A}_{ij} = a_i a_j A_{ij} S$$

$$\tilde{\phi}_{ij} = \phi_i - \phi_j + \phi_{ij}$$

- which can be solved when the closure error is small

Phase calibration

- For the phase, the equation depends on the differences of phases
- one antenna is used as reference antenna with $\varphi_i=0$

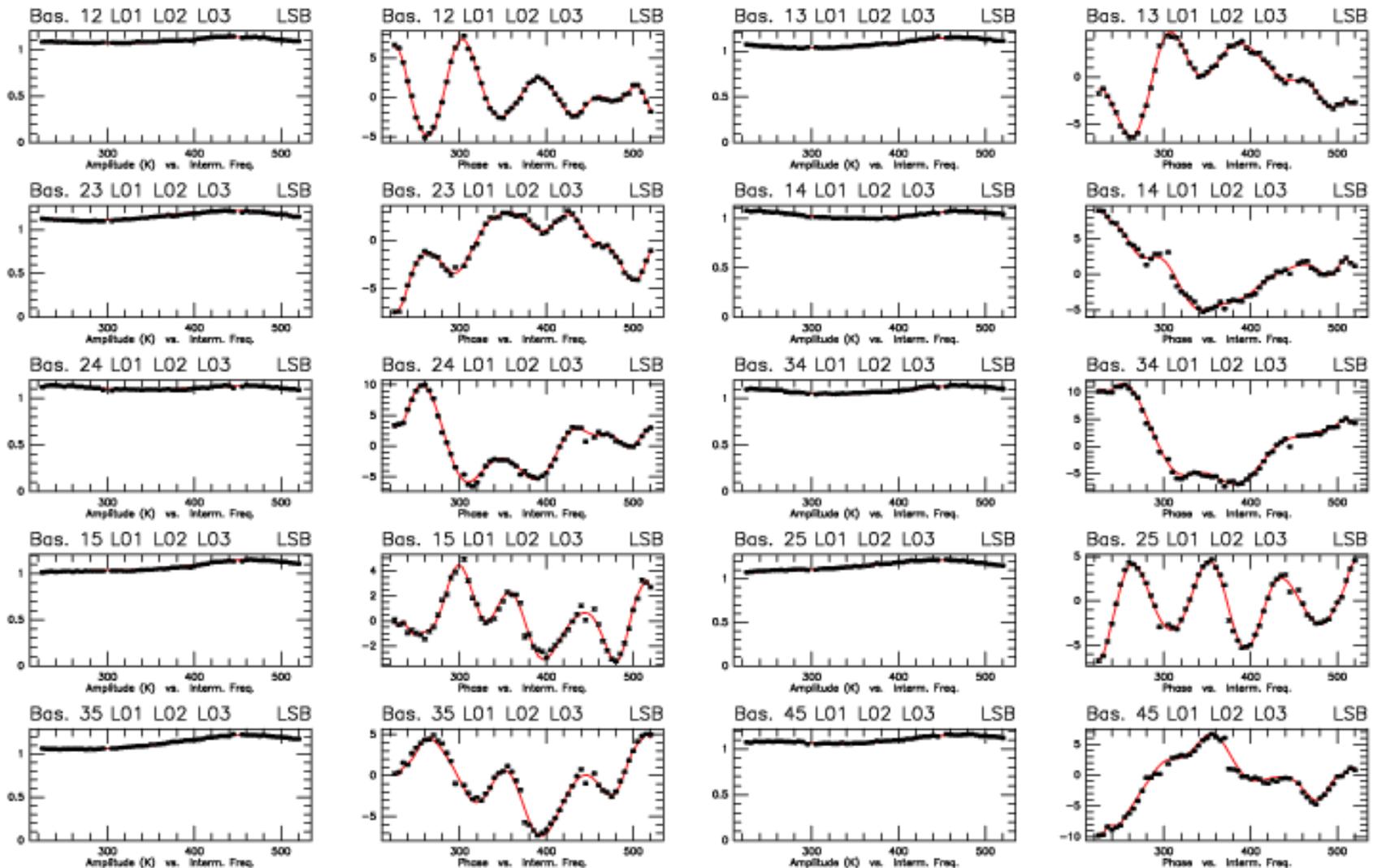
Bandpass and Flux calibration

- Bandpass
 - For spectral lines observations, one also has to calibrate the bandpass
 - use line-free, strong source and do long integration
- flux calibration
 - use source of known flux
 - tricky: planets are too big, they're resolved out
 - quasars are time variable

Example bandpass PdB - 3mm

KF: Uncal. CLIC - 19-MAY-1998 09:02:20 - schilke@champ N15N05W09W12E10
Am: Abs. 188 9866 H100 3C273 P CORR N2H+(10) 5C2 14-MAR-1998 01:16 .6
Ph: Rel.(A) Atm.

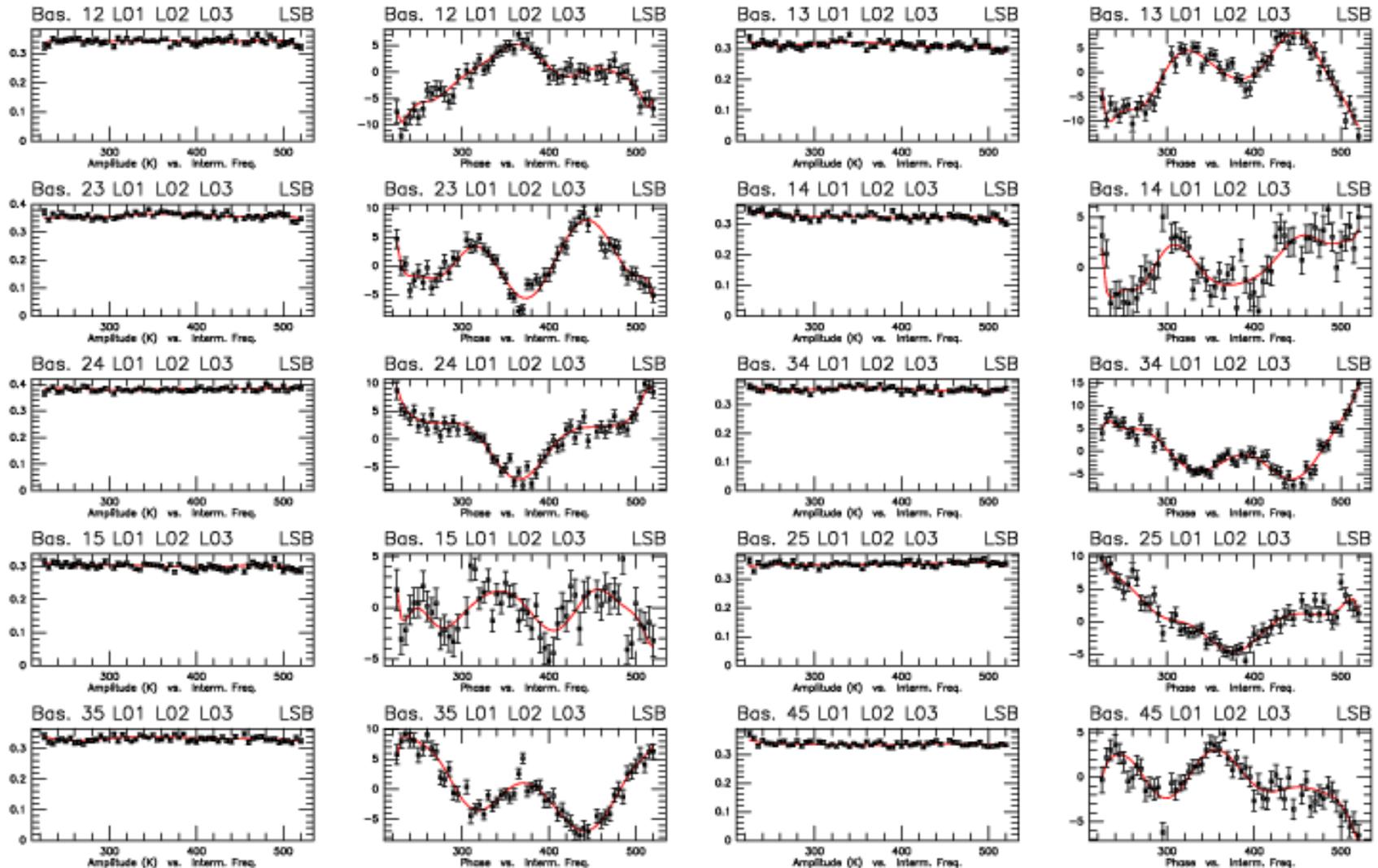
Scan Avg.
Vect.Avg.



Bandpass PdB 1mm - LSB

KF: Uncal. CLIC - 19-MAY-1998 09:03:14 - schilke@champ N15N05W09W12E10
Am: Abs. 1372 9866 H100 3C273 P CORR CO+(21) 5C2 14-MAR-1998 01:16 .6
Ph: Rel.(A) Atm.

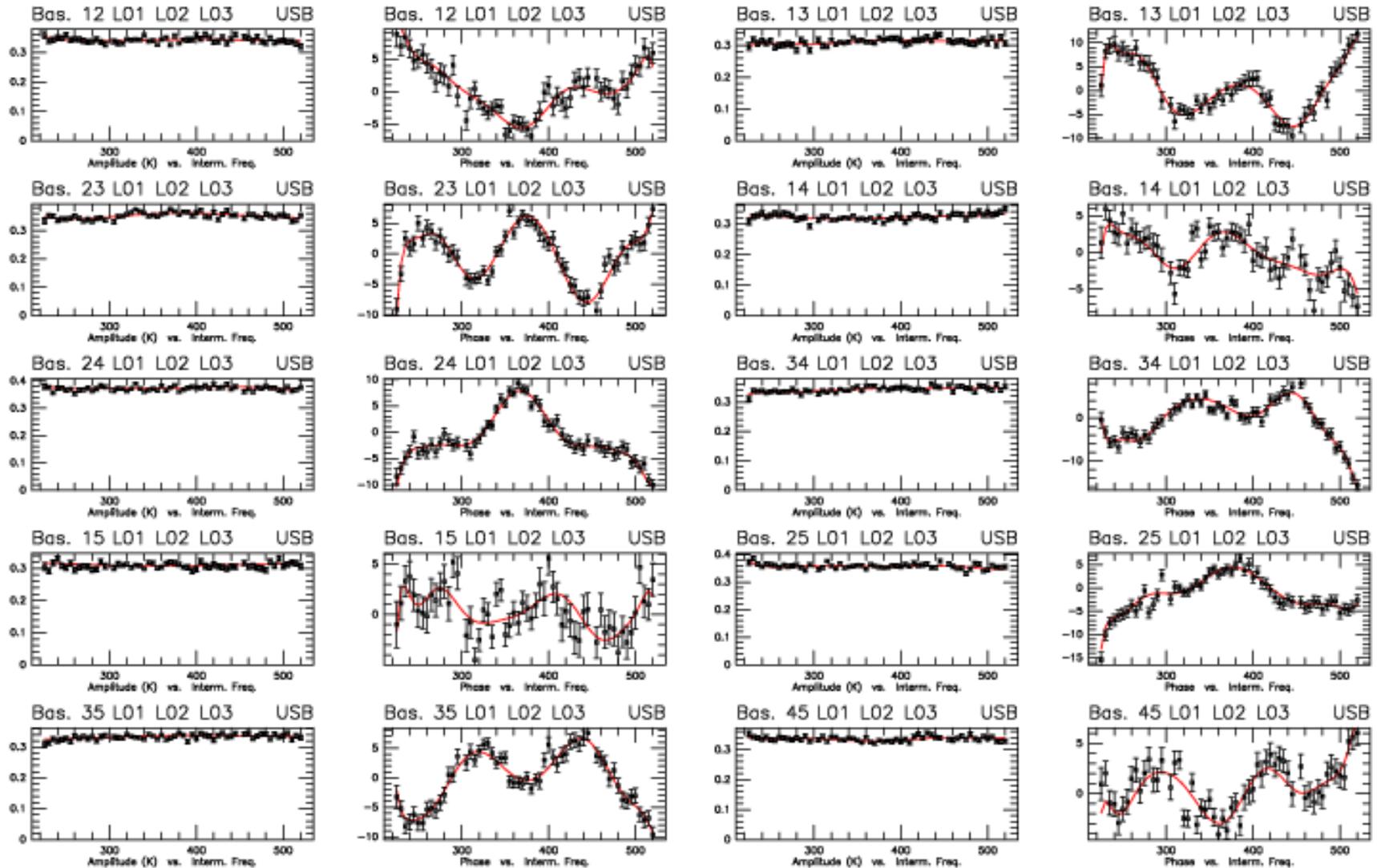
Scan Avg.
Vect.Avg.



Bandpass PdB 1mm - USB

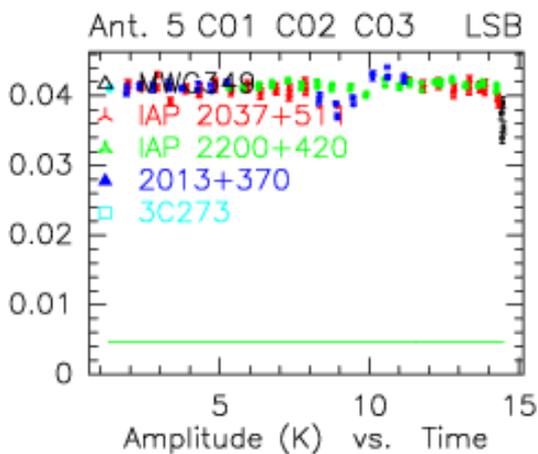
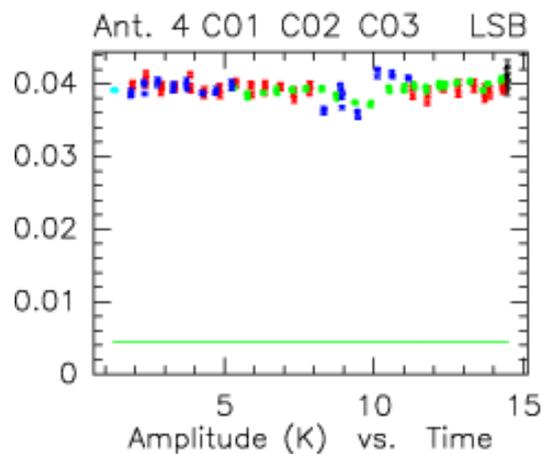
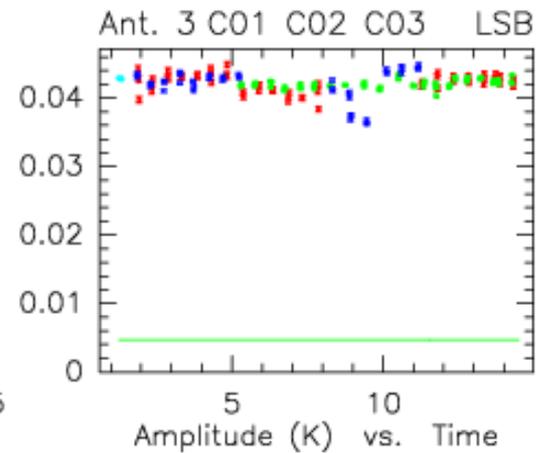
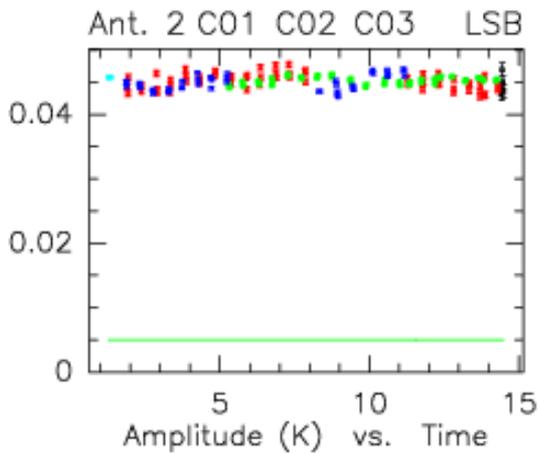
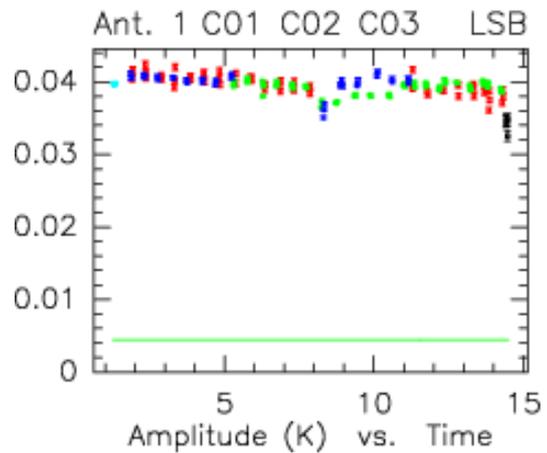
KF: Uncal. CLIC - 19-MAY-1998 09:04:41 - schilke@champ N15N05W09W12E10
Am: Abs. 1372 9866 H100 3C273 P CORR CO+(21) 5C2 14-MAR-1998 01:16 .6
Ph: Rel.(A) Atm.

Scan Avg.
Vect.Avg.



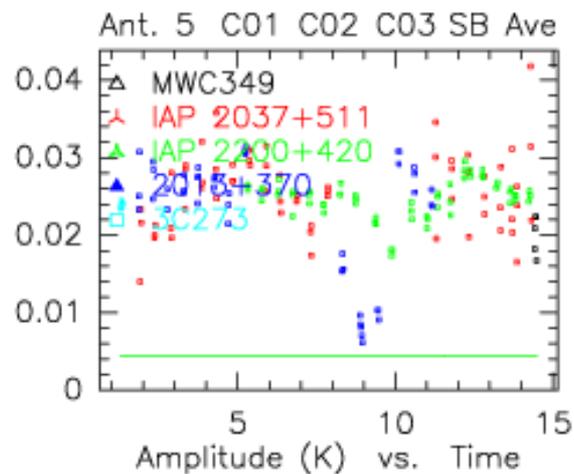
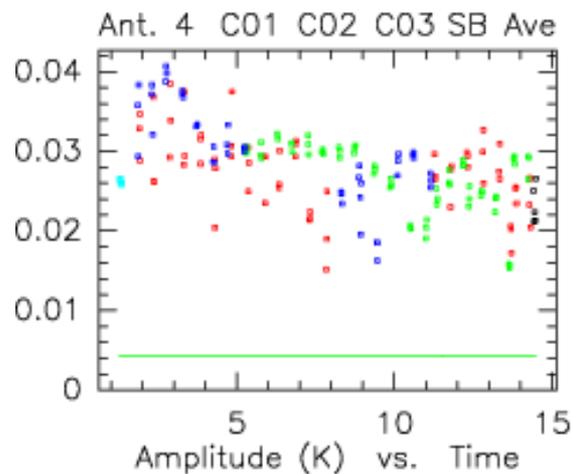
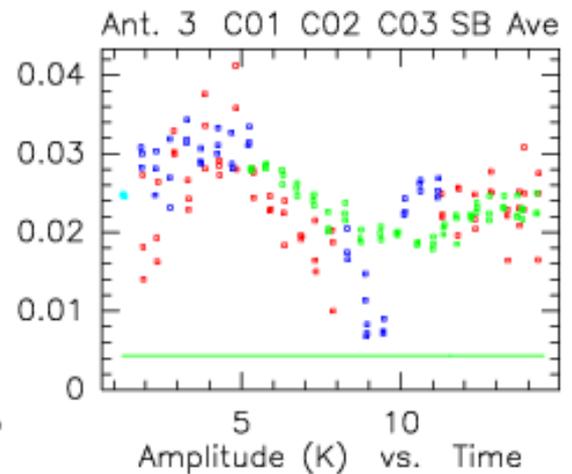
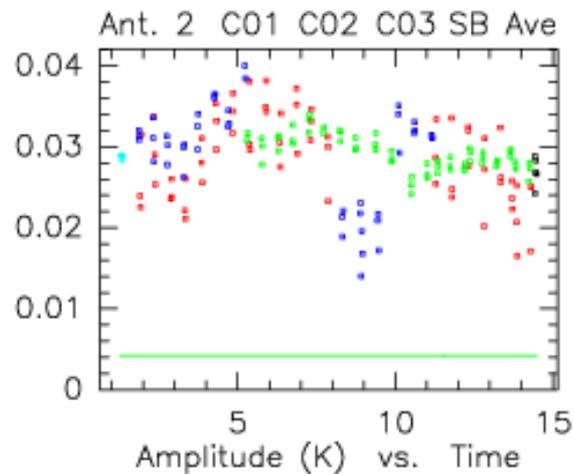
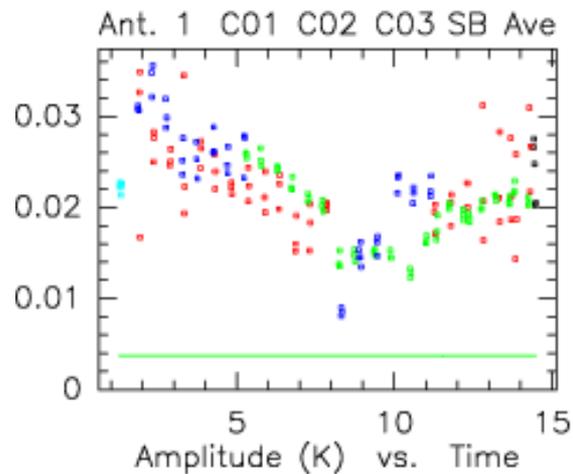
Flux calibration PdB 3mm

Am: Scaled 188 9866 H100 3C273 P CORR N2H+(10) 5C2 14-MAR-1998 01:16 .6 Vect.Avg.
 Ph: Rel.(A) Atm. 1184 725 H100 MWC349 O CORR N2H+(10) 5C2 14-MAR-1998 14:28 5.8



Flux calibration PdB 1mm

Ant: Scaled 1372 9866 H100 3C273 P CORR CO+(21) 5C2 14-MAR-1998 01:16 .6 Vect.Avg.
 Ph: Rel.(A) Atm. Ext. 2368 725 H100 MWC349 O CORR CO+(21) 5C2 14-MAR-1998 14:28 5.8



Interferometric Calibration & Imaging

Peter Schilke, MPIfR

Lecture

is available on

<http://www.astro.uni-bonn.de/~bertoldi/wiki/Radiolnterferometry>

Imaging

$$A_v(l, m) I_v(l, m) = \iint V_v(u, v) e^{-2\pi i(ul+vm)} du dv$$

in reality, with incomplete sampling

$$I_v^D(l, m) = \iint V'_v(u, v) S(u, v) e^{-2\pi i(ul+vm)} du dv$$

direct Fourier transform of all M points of the (u, v) plane

$$I_v^D(l, m) = \frac{1}{M} \sum_{k=1}^M V'_v(u, v) e^{-2\pi i(u_k l + v_k m)}$$

Imaging

- and this on an $N \times N$ raster (in the sky plane)
- this requires $4MN^2$ multiplications or, since M is of order N^2 , $O(N^4)$ multiplications
- since N is of order 1000 or so, and one has to multiply with the number of spectral channels, this is a lot of calculations
- Alternative: interpolating on rectangular grid (gridding) and using Fast Fourier Transform, which is $O(N^2 \log_2 N)$

Sampling

Sampling function

$$S(u, v) = \sum_{k=1}^M \delta(u - u_k, v - v_k)$$

sampled visibility function

$$V^S(u, v) = \sum_{k=1}^M \delta(u - u_k, v - v_k) V'(u_k, v_k)$$

*Fourier transform of sampling function is the dirty beam
folding of true image with dirty beam gives dirty image*

Weighted sampling

Weighted sampling function

$$W(u, v) = \sum_{k=1}^M R_k T_k D_k \delta(u - u_k, v - v_k)$$

weighted sampled visibility function

$$V^W(u, v) = \sum_{k=1}^M R_k T_k D_k \delta(u - u_k, v - v_k) V'(u_k, v_k)$$

Weighting terms

- R_k : weighting for quality of data
 - system temperature
 - integration time
 - bandwidth
- T_k : tapering function
 - downweighting of outer points
 - cleaner, but larger beam
- D_k : density weighting
 - takes into account clumping of data
 - $D_k = 1$: natural weighting: better sensitivity
 - $D_k = 1/N_s(k)$: uniform weighting: $N_s(k)$ is number of data points in region of width s : higher resolution

Gridding

- Folding with function C

$$V^R(u, v) = \sum_{k=1}^M C(u_c - u_k, v_c - v_k) V^W(u_k, v_k)$$

where C is a function which is identical to zero outside a small region

$$V^R(u, v) = R(C * W) = R(C * (WV'))$$

where R is a resampling function

$$R(u, v) = \sum_{j=-\infty}^{\infty} \sum_{k=-\infty}^{\infty} \delta(j - u/\Delta u, k - v/\Delta v)$$

where Δu and Δv define the cell size

Resampling

using the convolution theorem

$$\tilde{I}^D = \overline{V}^R = \overline{R} * (\overline{C} \overline{V}^W) = \overline{R} * [\overline{C} * (\overline{W} \overline{V}')]]$$

R is its own fourier transform

$$\overline{R}(l, m) = \Delta u \Delta v \sum_{j=-\infty}^{\infty} \sum_{k=-\infty}^{\infty} \delta(j - l / \Delta u, k - m / \Delta v)$$

Resampling

- Resampling makes a periodic function out of I_D , with period $1/\Delta u$ in l and $1/\Delta v$ in m
- introduces *aliasing*: sources outside the field of view are folded into the field of view (through sidelobes of the dirty beam)
- One has to do the *gridding correction*:

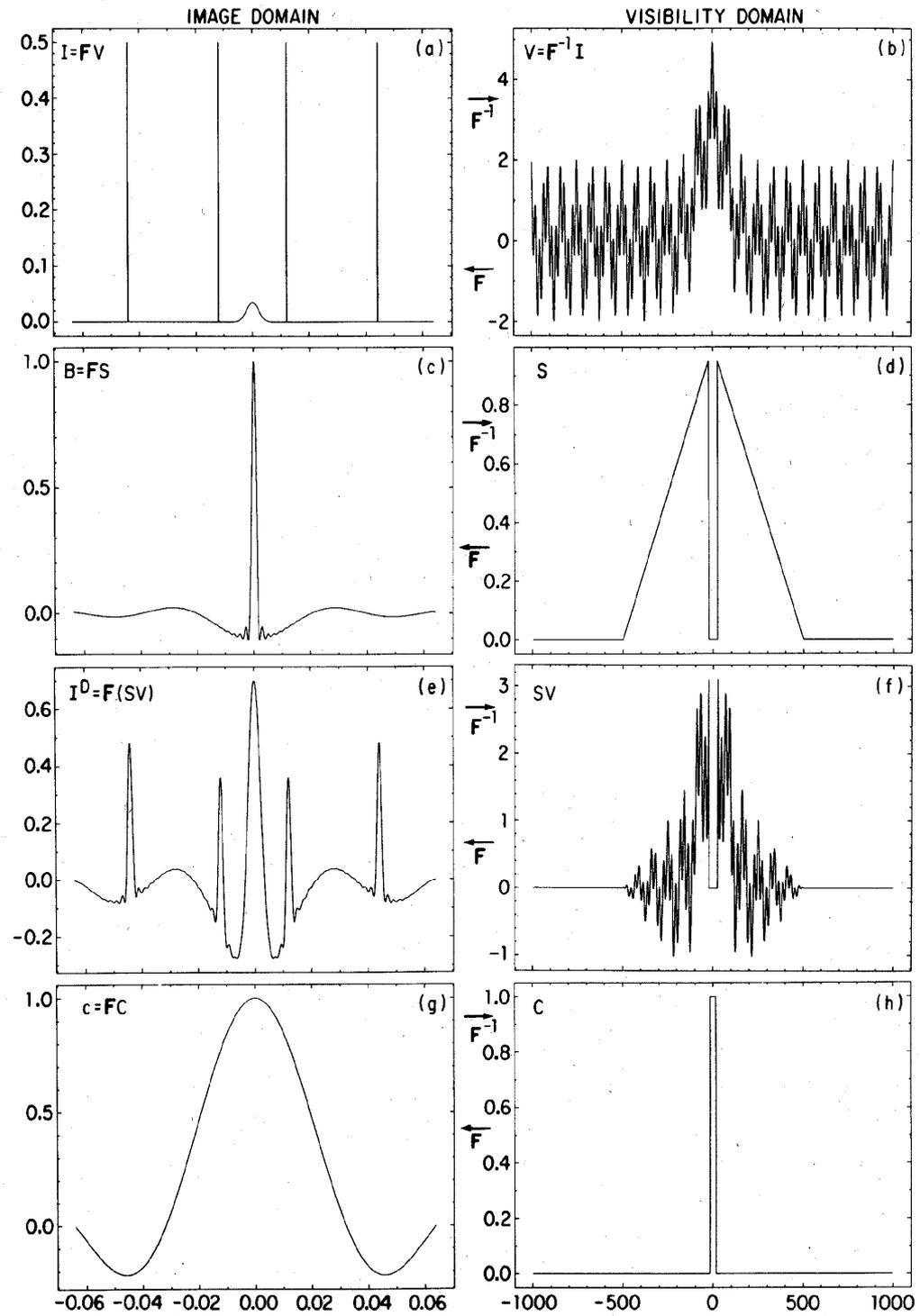
$$\tilde{I}_c^D(l, m) = \frac{\tilde{I}^D(l, m)}{\bar{C}(l, m)} \quad \text{for the dirty image}$$

$$\tilde{B}_c^D(l, m) = \frac{\tilde{B}^D(l, m)}{\bar{C}(l, m)} \quad \text{for the dirty beam}$$

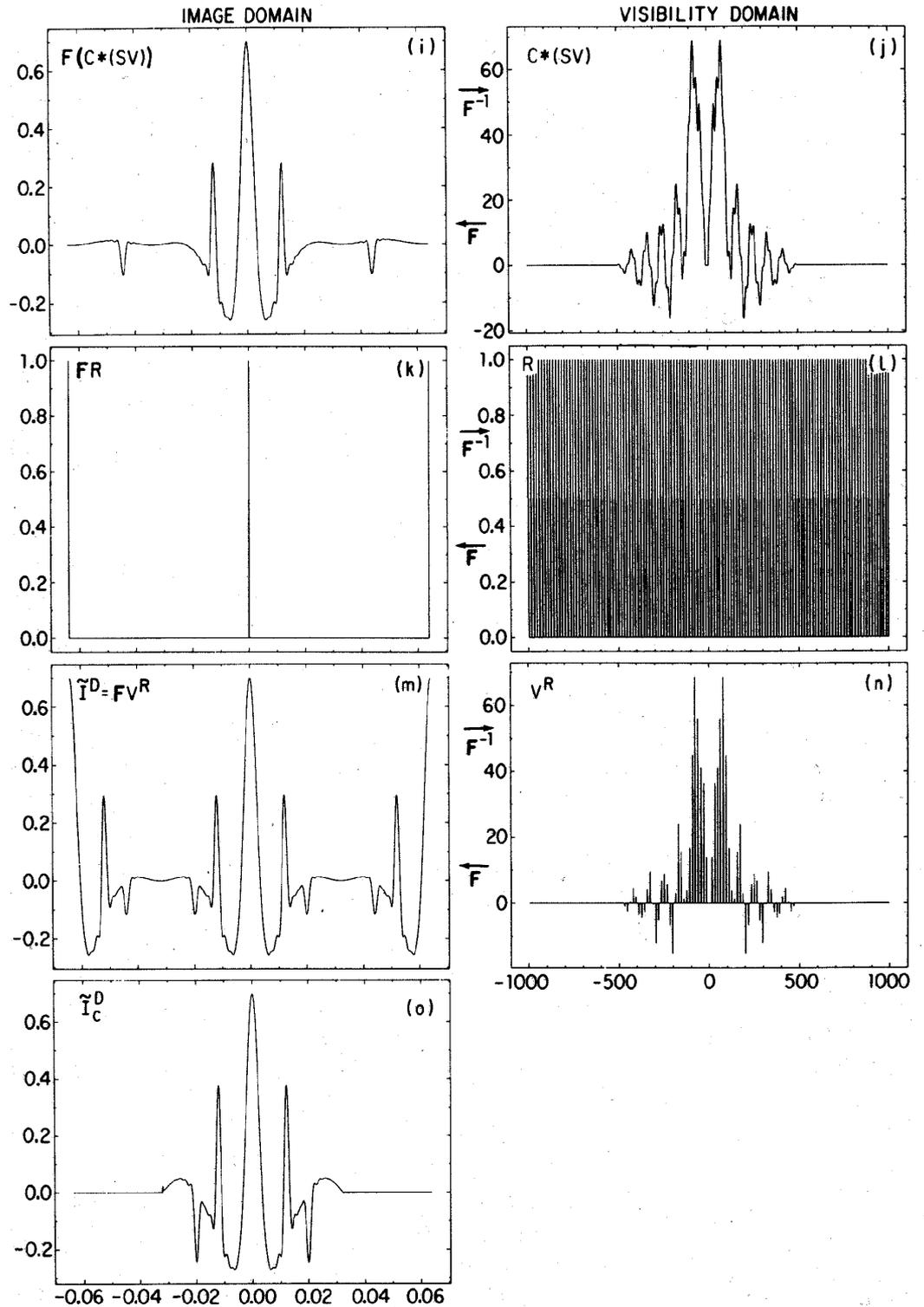
Gridding functions

- Hat box (square)
 - advantage: fast
 - disadvantage: bad sidelobes, lots of aliasing
- exponential, Gaussian:
 - suppression of aliasing
- Sinc (fourier transform of hat box, i.e. hat box in fourier plane)
- exponential times sinc

Gridding



Gridding



Visibility sampling

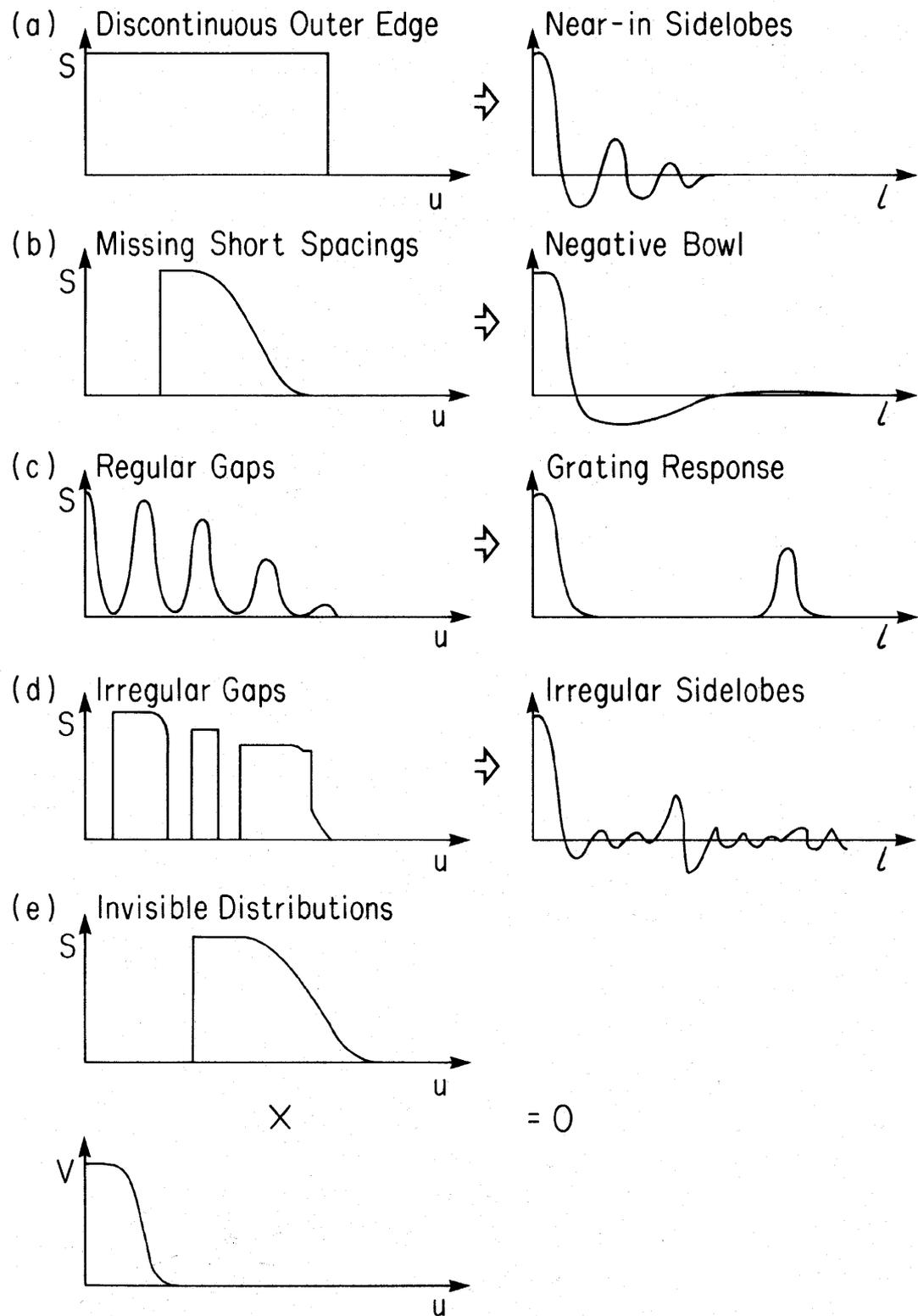


Image restoration

- Goal: “true” image of the sky
- Problems
 - convolution with dirty beam
 - missing spatial frequencies
- Restoration algorithms
 - CLEAN type
 - MEM type

CLEAN

- find amplitude and coordinates of maximum in dirty image (can be restricted to certain areas)
- subtract dirty beam from position of maximum, multiplied with amplitude times loop gain (< 1)
- repeat until residuum is below a certain amplitude limit or maximum number of components has been reached
- convolve all found components with clean beam (elliptical Gaussian fitted to center of dirty beam) and add them up
- add residuum of dirty map

MEM

- Uses model, convolves with dirty beam and minimizes

$$\chi^2 = \frac{\sum_r |V(u_r, v_r) - \hat{V}(u_r, v_r)|^2}{\sigma_{V(u_r, v_r)}^2}$$

while at the same time minimizing the Entropy

$$H = - \sum_k I_k \ln I_k$$

- to select the “simplest” model compatible with the data

Comparison

- CLEAN is well suited for small arrays, but deals badly with extended emission
 - new developments: multiscale clean
- MEM is computing intensive, but can use models (e.g. from single dish maps) and does extended emission well
- hybrids do exist

UV fitting

- To avoid problems with gridding etc. one can also fit source models directly in the (u,v) plane
- works well, but only for simple geometries (Gaussians, disks, toroids)

Sensitivity

- Sensitivity of single dish telescope

$$\Delta T_A = \frac{f T_{sys}}{\sqrt{t \Delta \nu}}$$

- where f depends on the measurement method (e.g. $f = \sqrt{2}$ for position switching), also absorbs efficiency losses from clipping and A2D conversion in correlators

Sensitivity

- or, in flux density units

$$\Delta S_{\nu} = \frac{f 2 k T_{sys}}{A_e \sqrt{t \Delta \nu}}$$

- for interferometers there are N telescopes and $N(N-1)/2$ baselines and correlations and each correlation increases the noise by a factor $\sqrt{2}$

$$\Delta S_{\nu} = \frac{f 2 k T_{sys}}{A_e \sqrt{N(N-1)t \Delta \nu}}$$

Sensitivity

- Inserting numbers, one finds

$$\Delta S_{\nu} = 1.44 \frac{f T_{sys}}{A_e \sqrt{N(N-1)t \Delta \nu}}$$

$$\Delta T_b = 19.2 \frac{f \lambda^2 T_{sys}}{A_e \theta^2 \sqrt{N(N-1)t \Delta \nu}}$$

with λ in mm, θ in arcsec and $\Delta \nu$ in kHz

Units for ΔS_{ν} are Jy/beam and for ΔT_b Kelvin

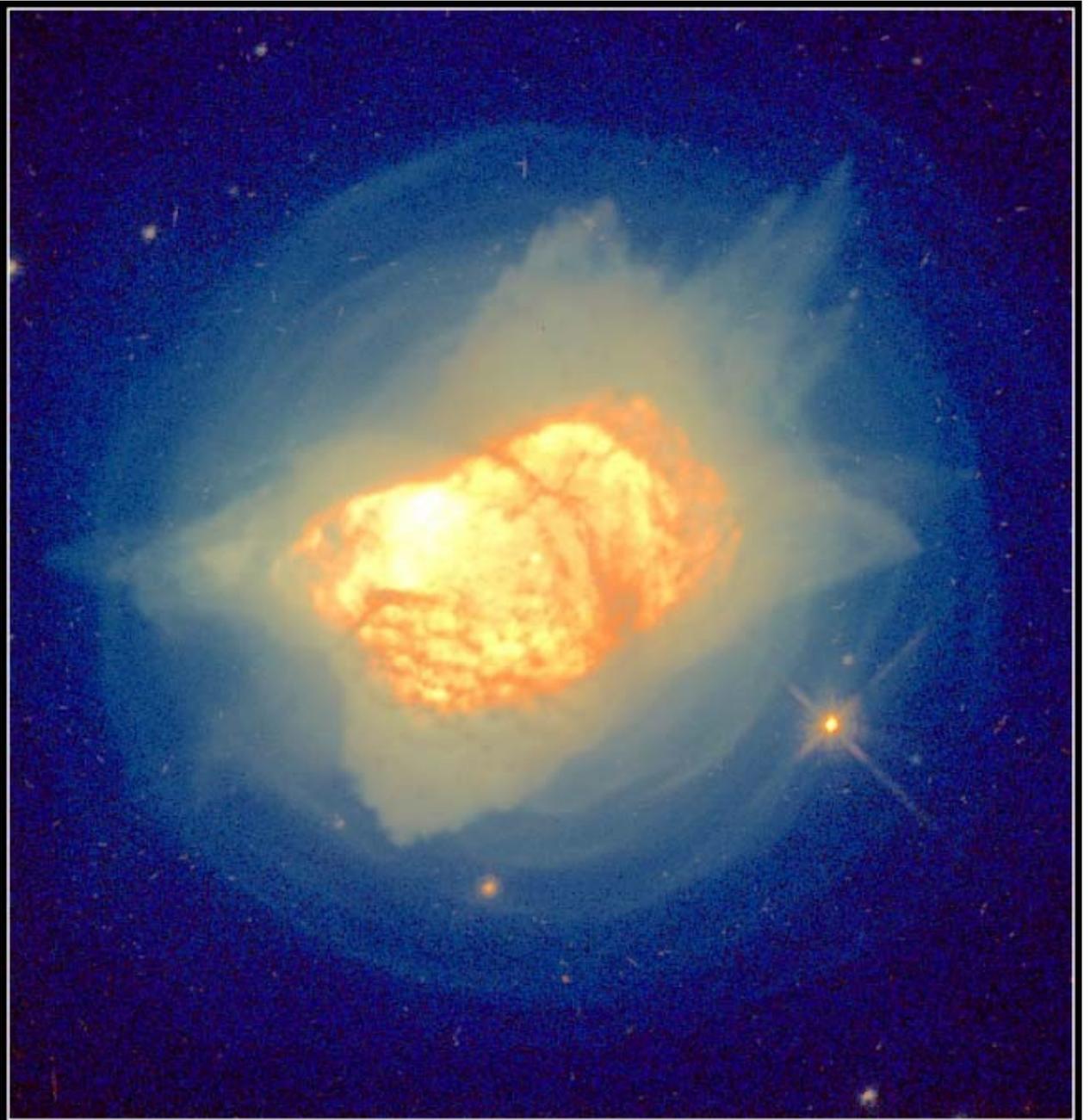
Sensitivities

- Sensitivities in flux depend only on antenna area, integration time and bandwidth
- Sensitivities in temperature depend on beam size, for very small beam size one has a very low brightness temperature sensitivity

Examples

- Two examples from Plateau de Bure
 - NGC7027
 - planetary nebula at high declination
 - good (u,v) coverage
 - G10.47
 - high-mass star forming region at low declination (-20°)
 - bad (u,v) coverage

NGC7027
optical

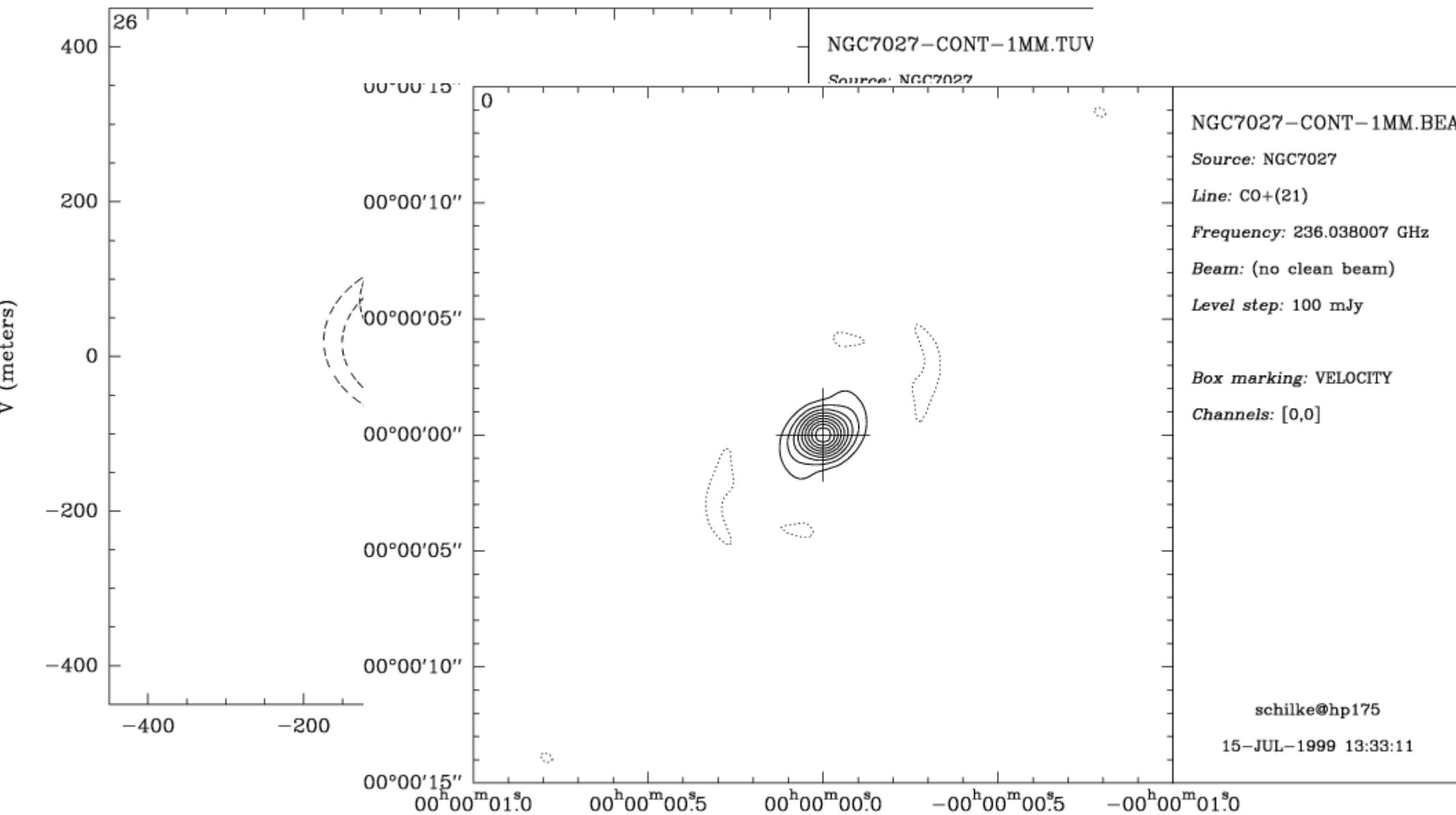


Planetary Nebula NGC 7027

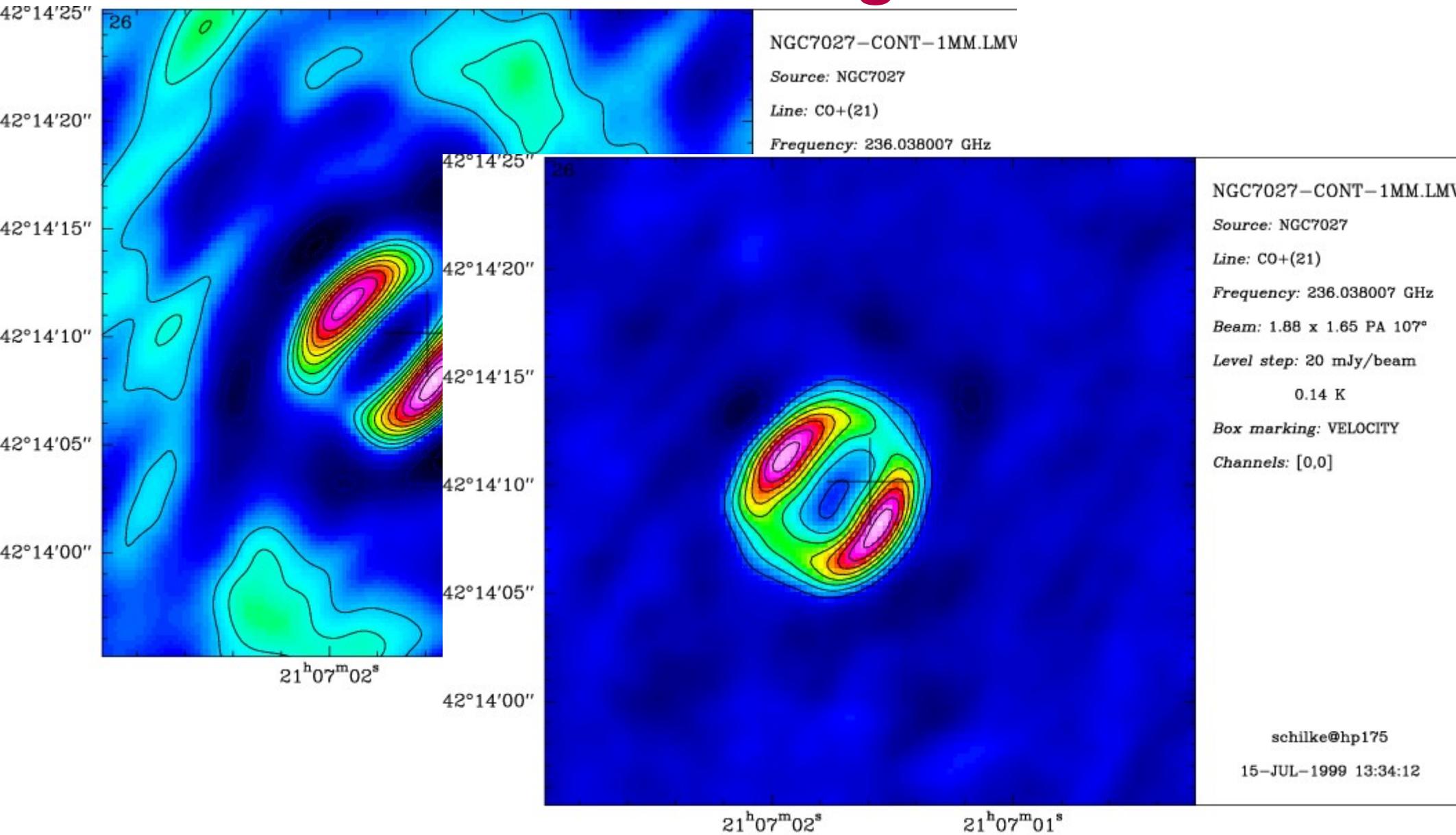
HST · WFPC2

PRC96-05 · ST ScI OPO · January 16, 1996 · H. Bond (ST ScI) and NASA

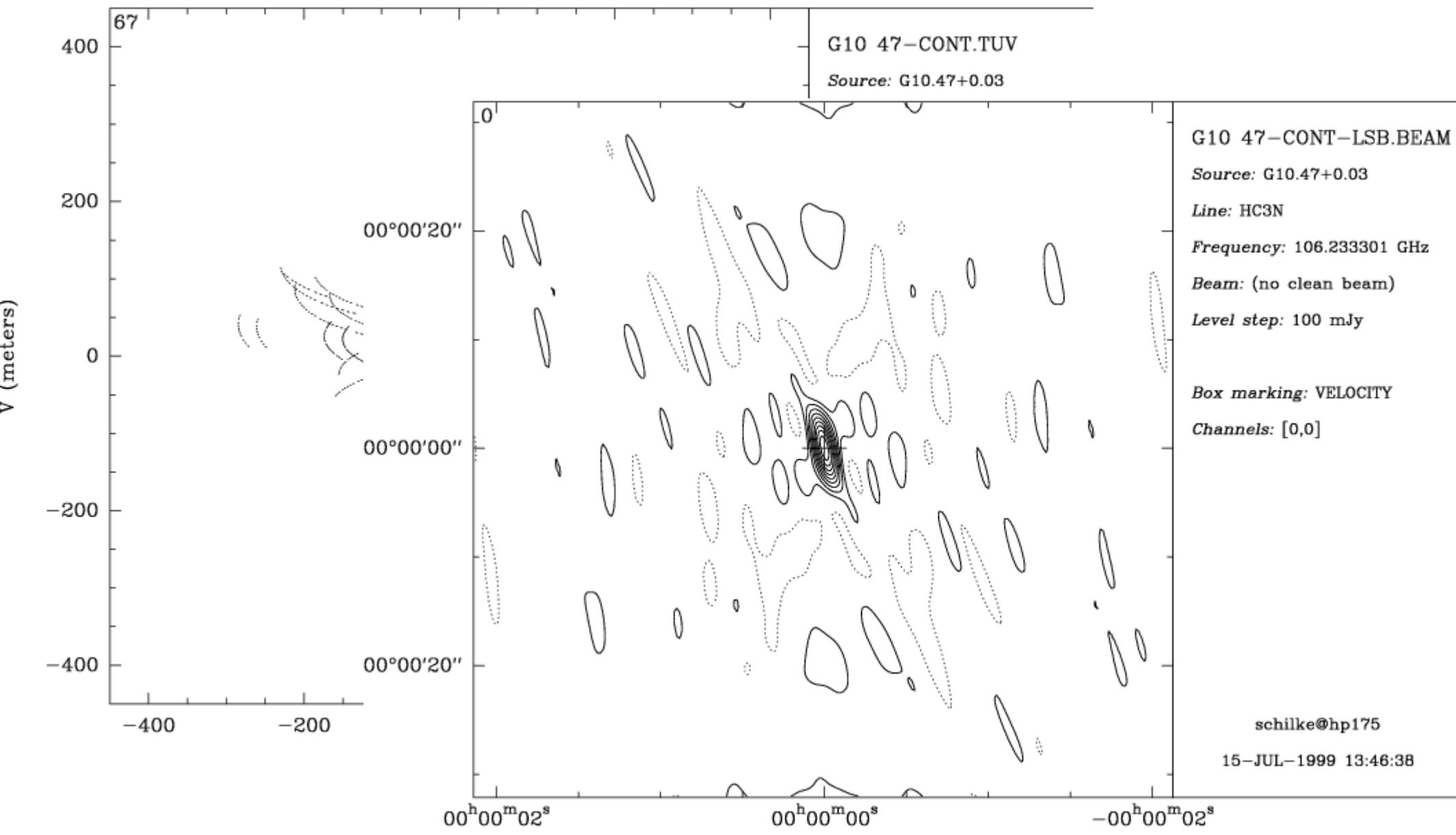
Good beam



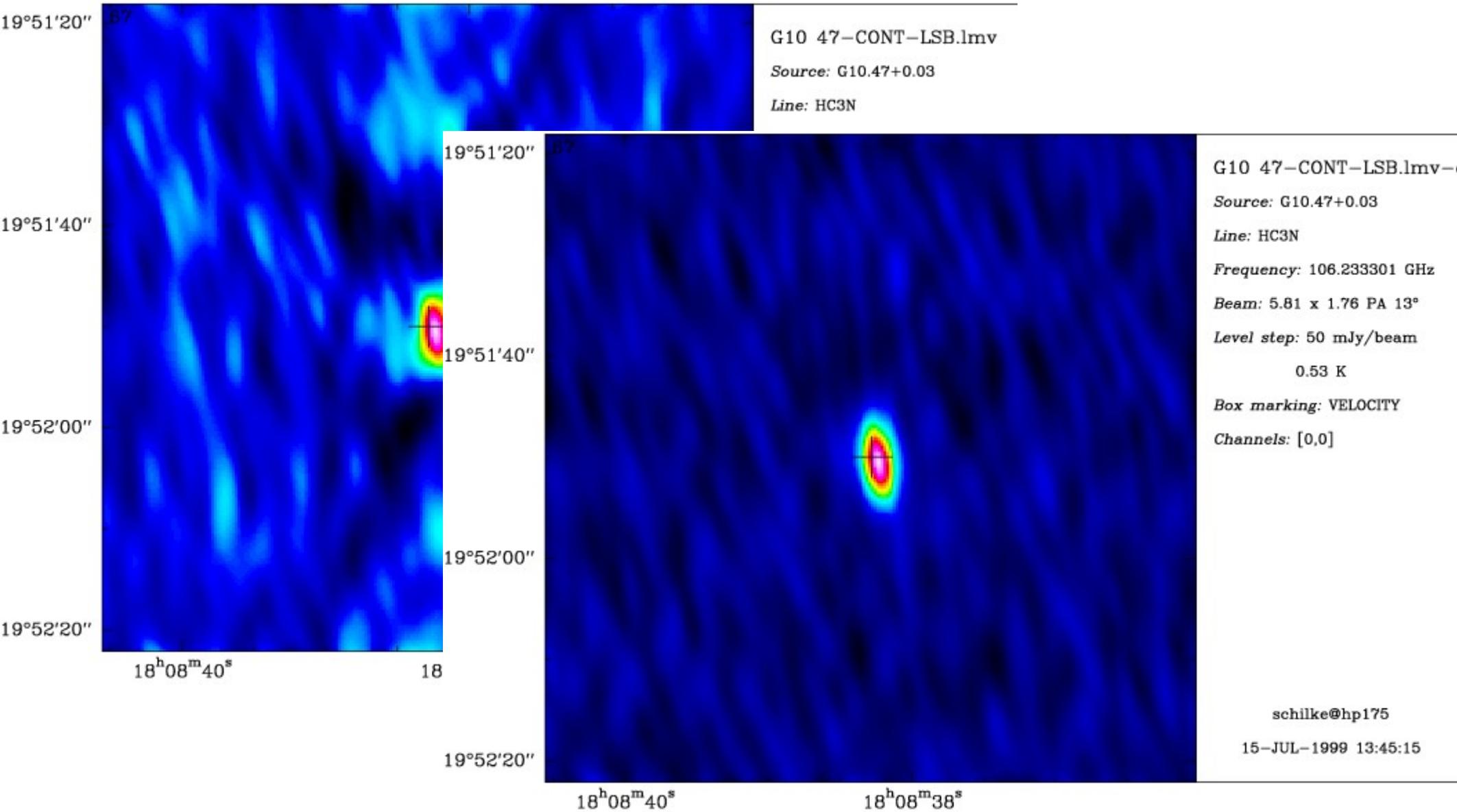
Good image



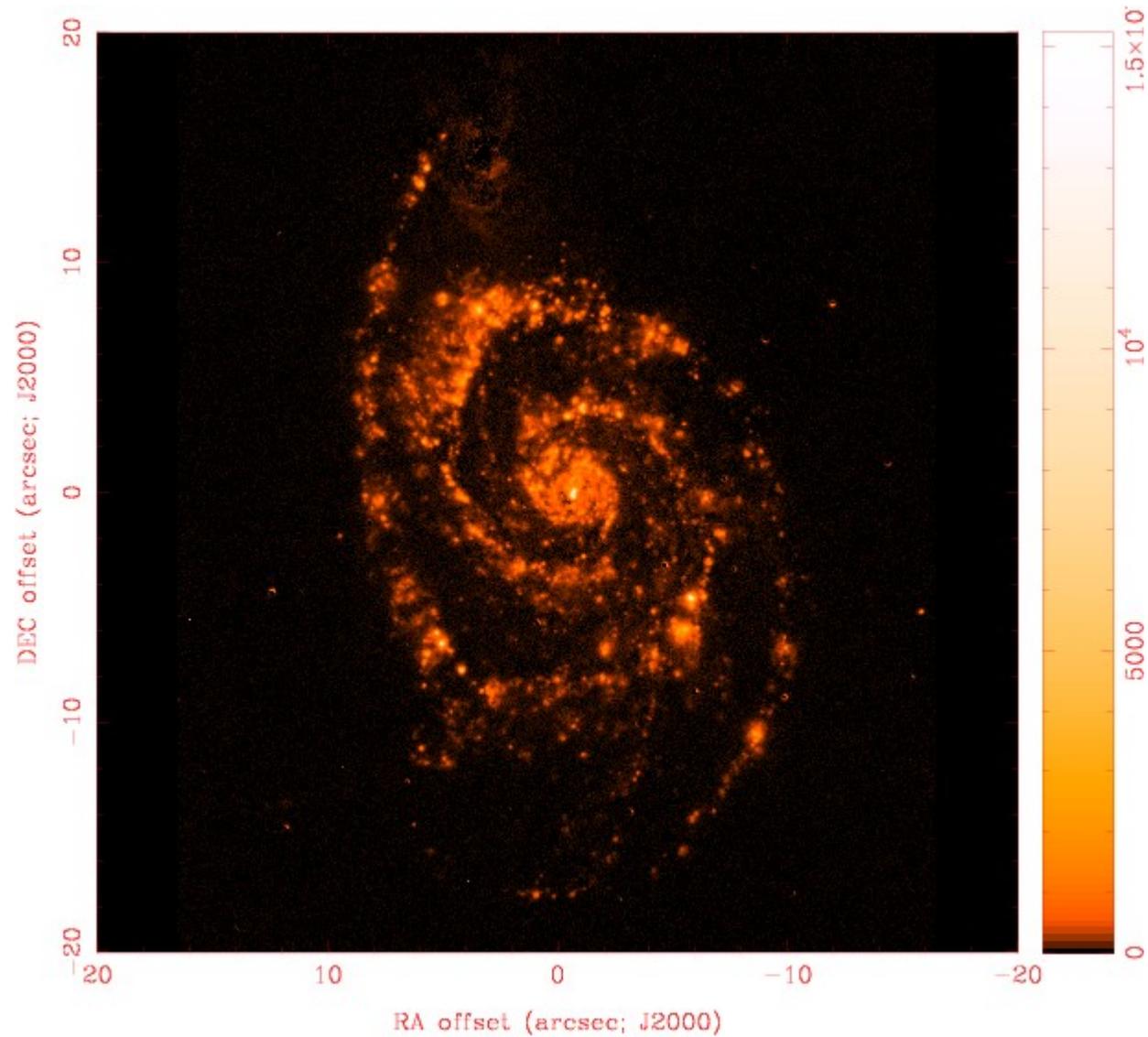
Bad beam



Bad image



further examples: simulations



Bad (u,v) coverage

I p1.30.M51.0.04.uv 230.0000 GHz

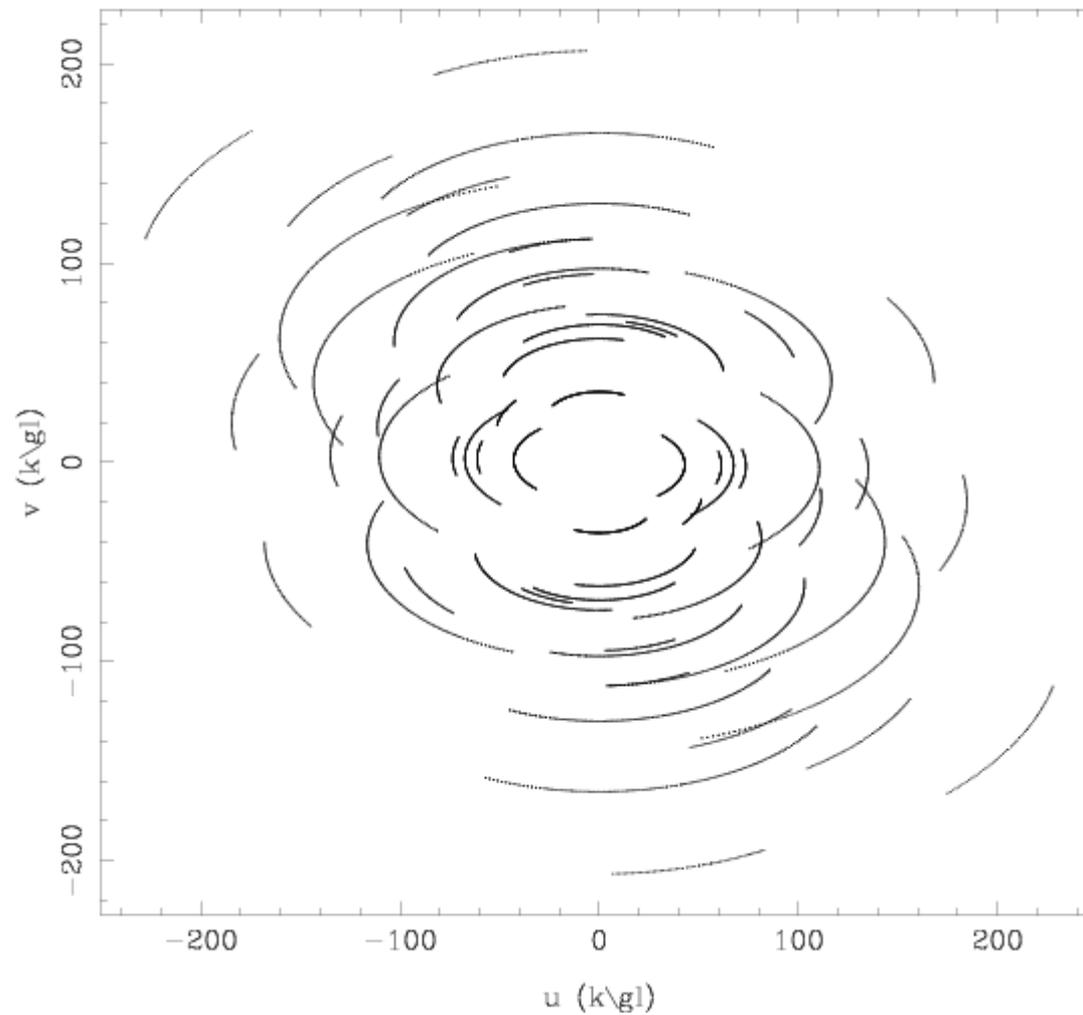
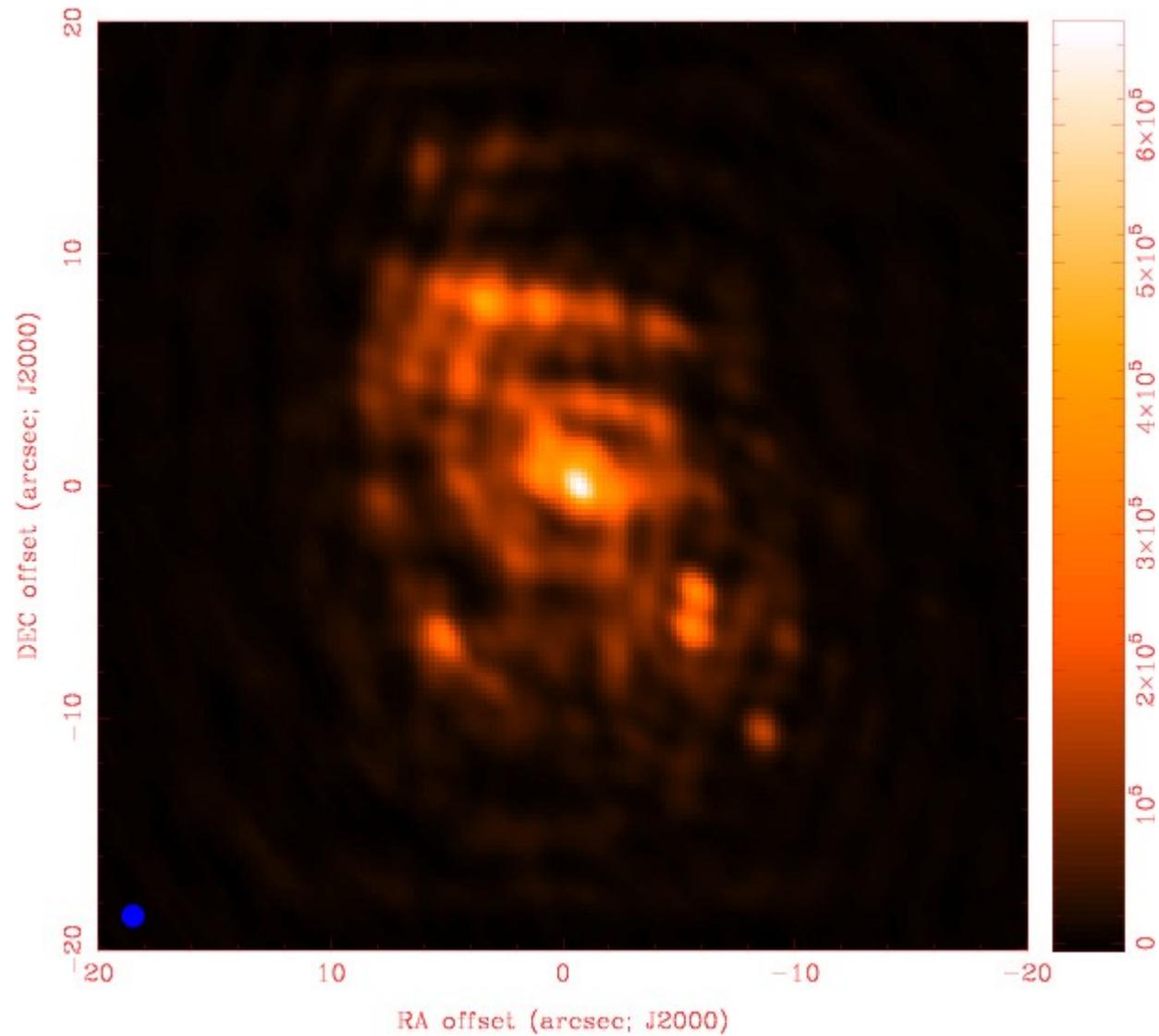
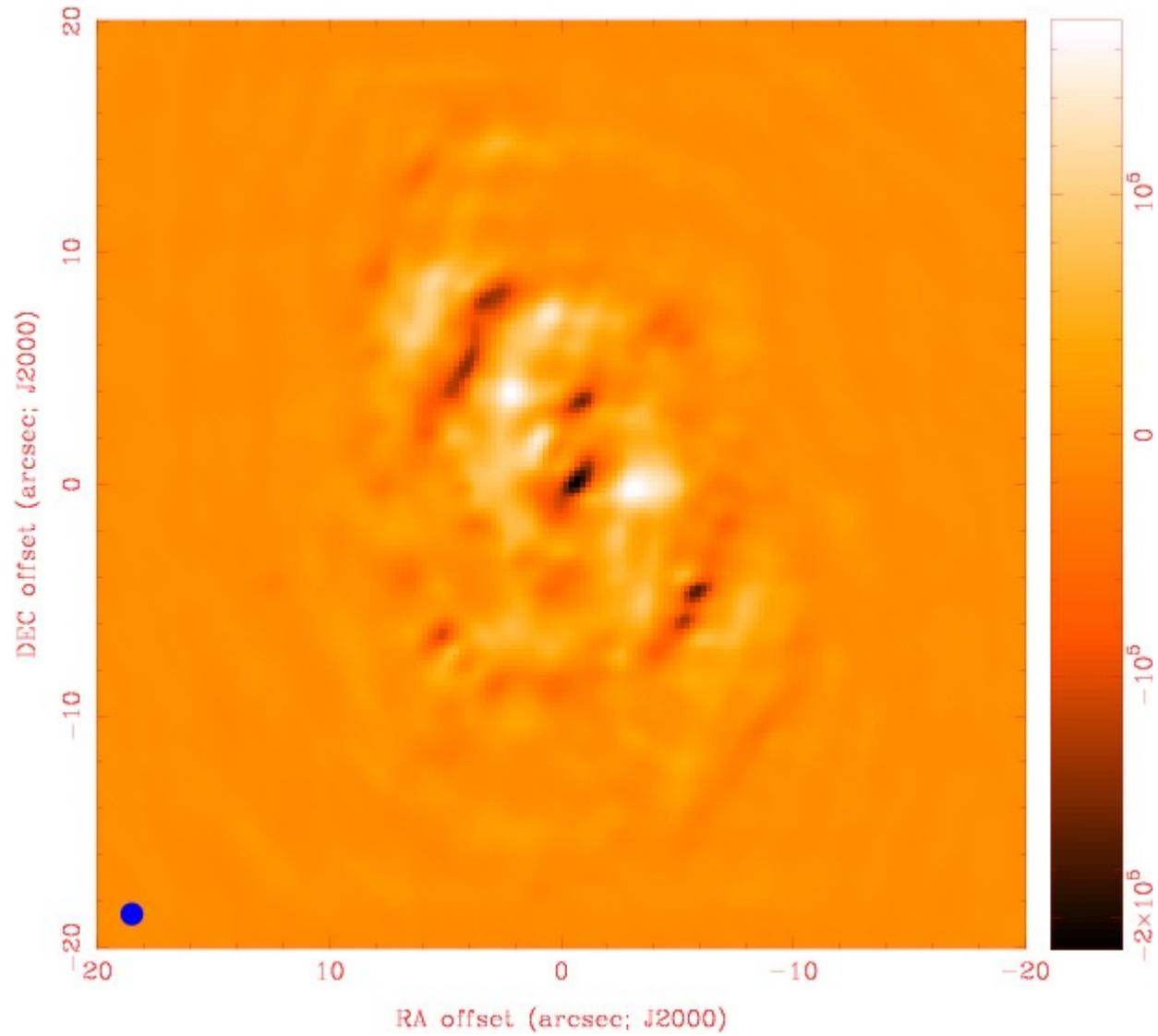


Image (including short spacings)



Residual



Better (u,v) coverage

I p1.30.M51.0.04.uv 230.0000 GHz

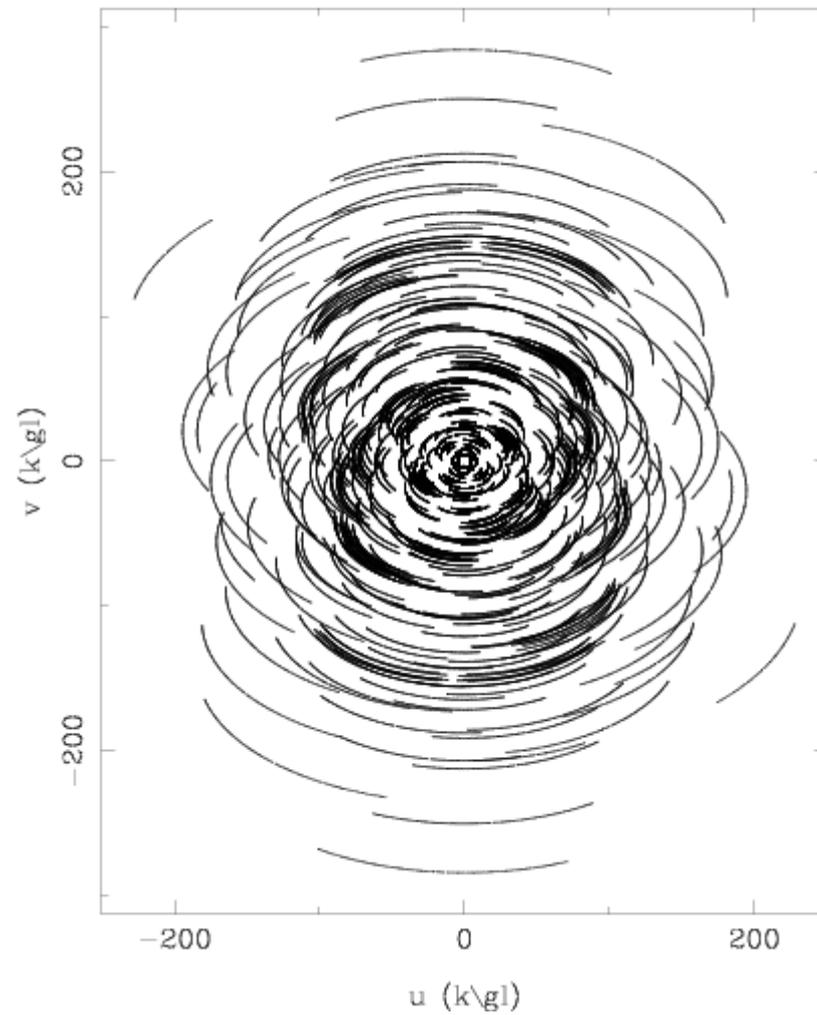
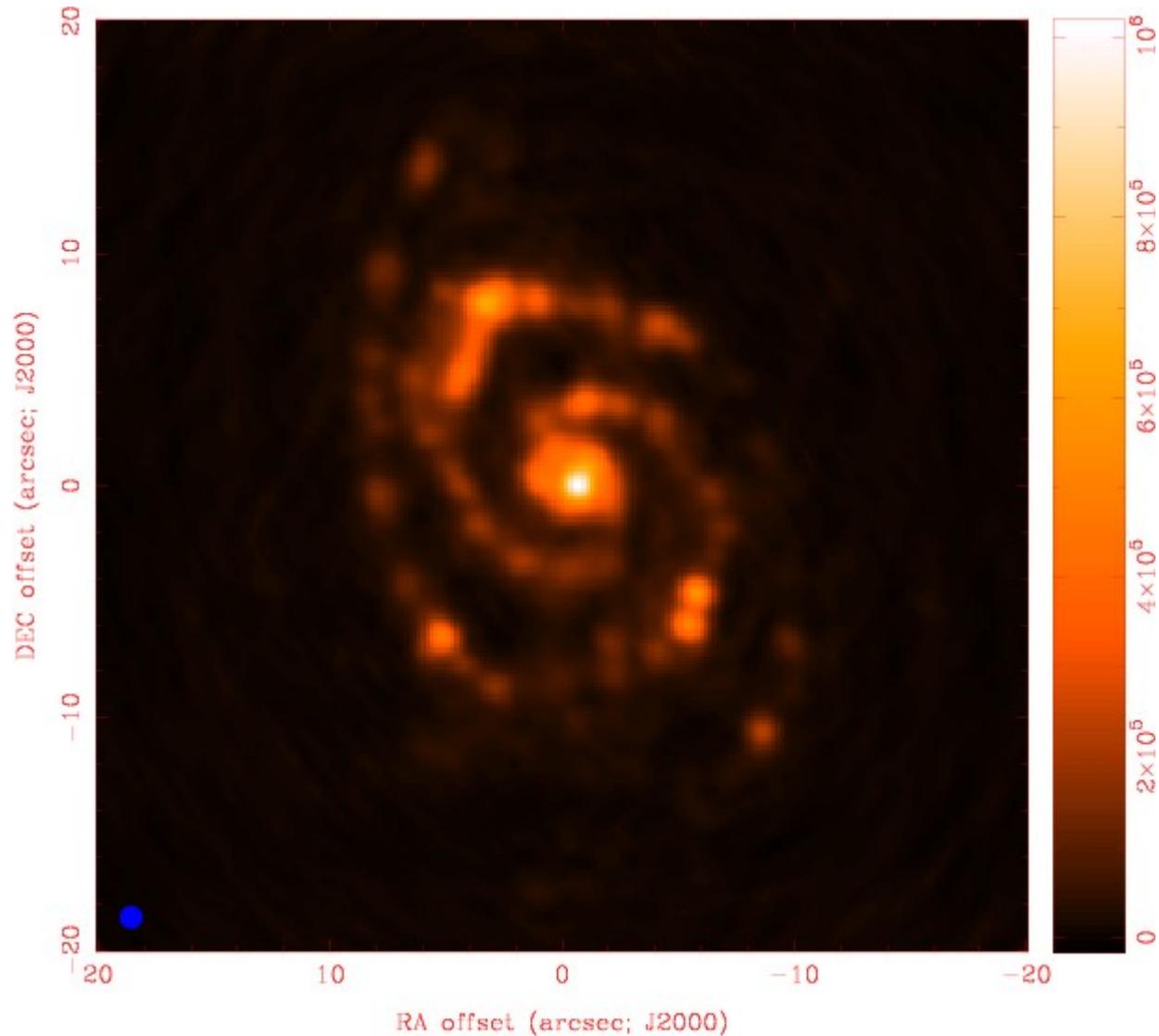
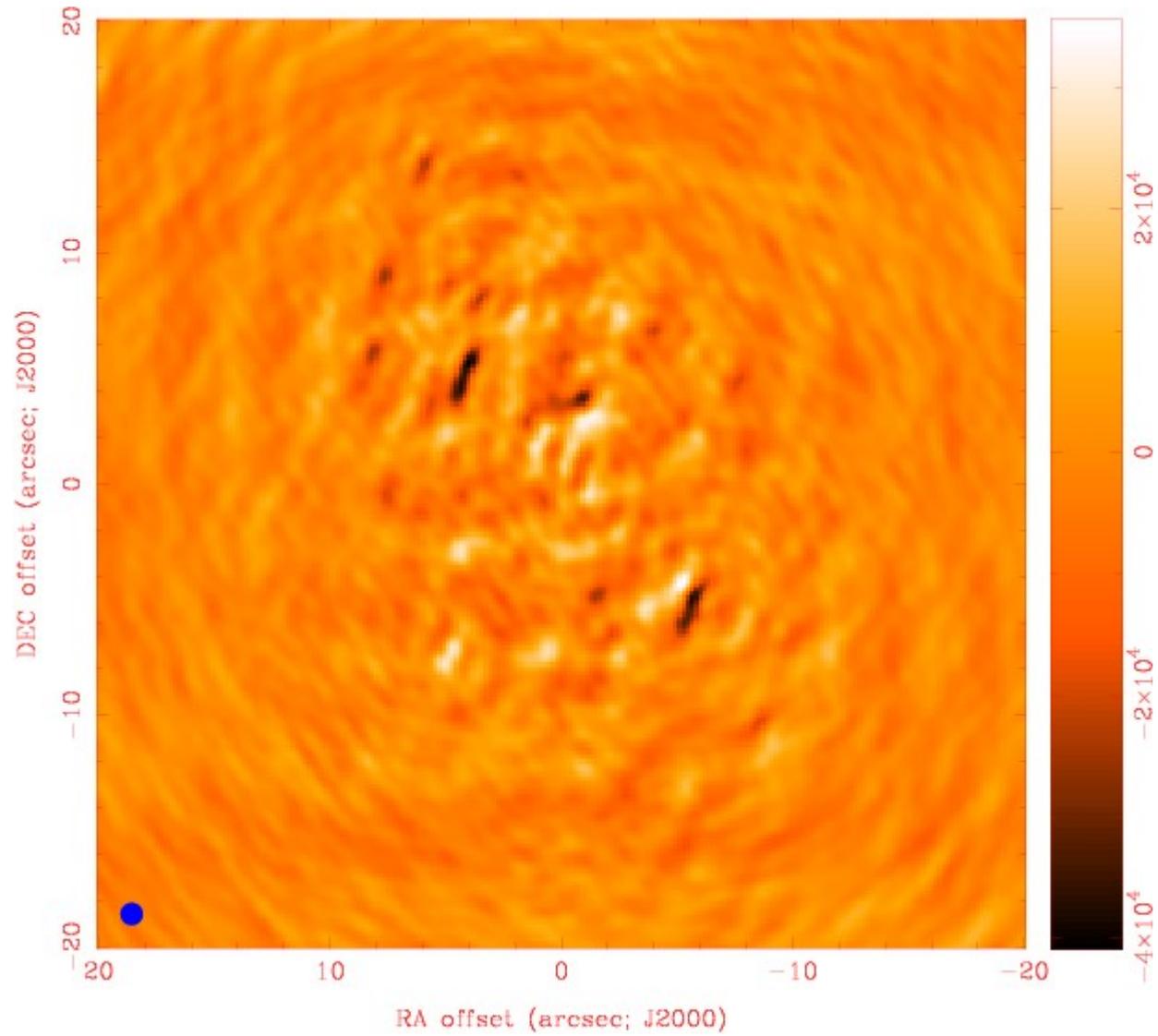


Image (including short spacings)



Residual



Interferometers



ALMA

